

Petrolog 4

Manual

Version 4.2.6
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Friendly Solutions

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Technical requirements, installation, and licencing

Petrolog4 runs under Windows operating system (XP or higher). Screen resolution should be set to higher than 1400 x 1000 pixels.

The current release requires a computer with a 64-bit processor. If you require a 32-bit version of the software, please email support@petrologsoftware.com.

Note: Correct display of the Main form of Petrolog4 (Fig. 1) may require that the 'Text size' option in Display settings is set to 100% (in earlier versions of Windows, this is the DPI setting that should be set to 'Normal size' at Display Properties/Settings/Advanced/General). To check/change this setting, go to the 'System' section of the Control Panel.

Installation

To instal the software, download Petrolog4.zip file from the website (petrologsoftware.com) and unpack its content into a folder on your computer.

Note: Petrolog4 would not work correctly if placed in a shared/managed folder, i.e., a folder that is administered by OneDrive, Dropbox, Google Drive, or other file sharing software. We suggest making a folder C:\Petrolog4 or C:\Programs\Petrolog4.

Note: Your computer must be connected to the internet when you start Petrolog4 for the first time. Start the program by double-clicking on Petrlog4.exe. When Petrolog4 starts for the first time, the Registration form will open requesting you to enter your Licence Key and User Key (Fig. 1).

The screenshot displays the Petrolog 4.0.5 software interface with the Registration dialog box open. The background window has tabs for 'Crystallisation', 'Reverse Crystallisation', 'Melt Liquidus Association', and 'Olivine MI'. The 'Crystallisation' tab is active, showing 'Models for phase-melt equilibrium' with a table of phases and models. The 'Extent of fractionation (%)' table is also visible. The 'Oxidation state' section shows calculation parameters. The 'Melt physical properties' section includes density and viscosity. The 'Calculation parameters' section shows the calculation step and output frequency. The 'Starting melt composition' table is at the bottom left. The Registration dialog box is centered, asking for User Key, Licence Key, Machine Key, Petrolog Version, Owner, and Expiry Date. It includes 'Ok', 'Reset', and 'Invalid Licence' buttons, and a link to the Petrolog website.

Phase	Model	P	W	Tr
Olivine	Ford et al. 1983	Y		
Plagioclase	Press to Select			
Clinopyroxene	Press to Select			
Orthopyroxene	Press to Select			
Pigeonite	Press to Select			
Spinel	Press to Select			
Ilmenite	Press to Select			
Magnetite	Press to Select			
Sulfide	Press to Select			
Fluid	Press to Select			

Phase	%fr
Olivine	100
Plagioclase	100
Clinopyroxene	100
Orthopyroxene	100
Pigeonite	100
Spinel	100
Ilmenite	100
Magnetite	100
Sulfide	100
Fluid	100

SiO2	TiO2	Al2O3	Fe2O3	FeO	MnO	MgO	CaO	Na2O
50.00	1.00	15.00	0.00	9.00	0.10	10.00	12.00	2.50

Figure 1. The Registration form of Petrolog4 before licence information is entered.

Once entered, click on the 'Ok' button to start using the software. Once licence is entered, you would not need to return to the Registration until the Licence Key expires. If you open the registration window, you will see your licence information (Fig. 2).

Note: Do not move any individual files unpacked from Petrolog4.zip to other folders on your computer, as this would result in a failure to start the program. If you would like to change the folder where Petrolog4 files are stored, copy all unpacked files to the new location.

The screenshot shows the Petrolog 4.0.5 software interface with the Registration dialog box open. The background window has tabs for 'Crystallisation', 'Reverse Crystallisation', 'Melt Liquidus Association', and 'Olivine MI'. The 'Crystallisation' tab is active, showing a table for 'Models for phase-melt equilibrium' and a table for 'Starting melt composition'. The 'Registration' dialog box is in the foreground, displaying the following information:

- Keys:**
 - User Key: [Empty field]
 - Licence Key: [Empty field]
 - Machine Key: F2C5DEE6D2C9
 - Petrolog Version: Petrolog 4.0.5
 - Owner: [Empty field]
 - Expiry Date: 2028-12-18
- Valid Licence:** Indicated by a green checkmark icon.
- Buttons:** 'Ok', 'Reset', and 'Exit Petrolog'.
- Links:** 'To obtain or manage your Petrolog licence please visit: <https://norsci.com/petrolog>' and 'Icons from: <https://icons8.com>'.

Figure 2. The Registration form of Petrolog4 after licence information is entered.

If you have not purchased your Keys before downloading the software, you can click on the link at the top left corner of the Registration form (<https://norsci.com/petrolog>) that will take you to the webpage where you can register and obtain the Keys.

To close the software without entering the Keys, click on the 'Exit Petrolog' button.

Licensing

Petrolog4 licences can be purchased for a minimum of 1 year. A single licence can include several installations (licence allocations). The cost of the licence is determined by the number of years it covers and the number of installations it includes. One installation for one year costs AUD\$100 in 2026.

Each Petrolog4 installation is linked to the computer the software is installed on, and the user who installed the software on that computer. More details are provided on <https://norsci.com/?p=user-licences>.

Every time Petrolog4 is started, the program will attempt to connect to the server and validate the licence. If Petrolog4 starts when the computer is off-line, this installation enters an off-line grace period. Each

Petrolog4 licence allocation allows for a 30-day off-line grace period that is counted from the time the program last started when the computer it is installed on was online.

Note: If Petrolog4 have not been run for over 30 days, it will not work if the computer is off-line when the program starts.

Each licence has a 14-day expiration date grace period. If the licence is not renewed within 14 days, Petrolog4 will stop working.

Moving Petrolog4 licence allocations to a different computer or a different user on the same computer

If you have purchased a licence with a single allocation and would like to change the computer/user you use to run Petrolog4, you would need to logon to your account on norsci.com and deactivate the previous allocation. After that, you will be able to register your available allocation on a different computer and/or under a different user.

1. Overview of Petrolog4

Petrolog4 is software for modelling fractional and equilibrium crystallisation of silicate magmas at variable pressure, melt oxidation state and melt volatile contents.

Other calculation options include, Modelling reverse of fractional crystallisation, Modelling post-entrapment re-equilibration of melt inclusions in olivine, Normative Mineralogy, and Classification Diagrams.

Modelling of crystallisation in Petrolog4 is based on the concept of pseudo-liquidus temperatures (Nathan, Vankirk, 1978; Nielsen, Dungan, 1983; Ariskin et al., 1986). The method relies on the ability of mineral-melt equilibrium models to calculate liquidus temperature not only for the range of melt compositions where the minerals are stable, but also for melt compositions outside the stability regions of each mineral (i.e., pseudo-liquidus temperatures).

The essence of the technique is to compare calculated pseudo-liquidus temperatures for a selected set of mineral species that may crystallize from a given melt composition. The mineral with the highest calculated temperature is considered the mineral on the liquidus of the given melt composition. This mineral is subtracted from melt, and then the process is repeated. The algorithm automatically determines the order of appearance of phases on the liquidus of the melt.

Note: Mineral-melt equilibrium models that can be included in Petrolog4 must calculate, at given values of pressure and oxygen fugacity, both the temperature at which the mineral appears on the liquidus of a given melt composition, and the composition of the mineral.

Minerals for which models meeting the above requirement are available in the current version are: olivine; plagioclase; clinopyroxene; orthopyroxene; pigeonite; spinel; magnetite; ilmenite; quartz; orthoclase; nepheline and leucite.

Additionally, Petrolog4 includes other phases for which phase-melt equilibrium models require that the temperature of the melt is independently known. Thus, including such phases in calculations requires that the liquidus temperature of the melt is established using appropriate mineral-melt equilibrium models described above.

Note: Phase-melt equilibrium models that can be included in Petrolog4 must calculate the composition of the phase at given values of pressure, temperature and oxygen fugacity.

Phases for which models meeting the above requirement are available in the current version are: immiscible sulphide melt; H₂O-CO₂ fluid, sulphate, apatite and zircon.

Compositions of all phases during calculations are fully mass- and charge-balanced for all elements including O. This allows for maintaining redox equilibrium between silicate melt, sulphide melt and H₂O-CO₂ fluid using available models of melt oxidation state as a function of pressure, temperature and oxygen fugacity. In the current version, such models are available for Fe and S, and thus these are the only elements that can have variable charges (Fe²⁺ and Fe³⁺ for Fe, S²⁻ and S⁶⁺ for S (note: oxidised S is S⁴⁺ when present in the fluid phase). Atomic weights, element charges and redox equilibria used in Petrolog4 are listed in Appendix 1.

Petrolog4 subdivides elements into three groups: major elements (Si, Ti, Al, Fe, Mn, Mg, Ca, Na, K, P and Cr), volatile elements (H, C, S, Cl, F, O) and trace elements (B, Be, Sc, V, Co, Ni, Cu, Zn, Ga, Rb, Sr, Y, Zr, Nb, Ru, Rh, Pd, Cs, Ba, La, Ce, Pr, Nd, Sm, Eu, Gd, Tb, Dy, Ho, Er, Tm, Yb, Lu, Hf, Ta, Re, Os, Ir, Pt, Pb, Th, U). During calculations, compositions of all phases can be displayed either as elemental concentrations or compound concentrations. Compound concentrations (either oxides or sulphides) are displayed for major and volatile elements only (see Section 2 for more details). Trace elements are always displayed using elemental concentrations.

Petrolog4 offers a model-independent algorithm (Danyushevsky and Plechov, 2011), which can incorporate a potentially unlimited number of:

- phase-melt equilibrium models for major, volatile and trace elements;
- solubility models for reduced and oxidised sulphur, fluid components and other elements in silicate melts;
- melt oxidation state models;

- models describing melt physical parameters such as density and viscosity;
- and other types of models.

Currently available models are listed in Appendix 1.

Note: *It is the responsibility of the user* to ensure that the models chosen for each calculation are appropriate for the chosen melt composition and calculation parameters such as pressure and oxygen fugacity. Applying any of the models outside the range of their applicability (as described in the referenced publications) may lead to incorrect results.

1.1. Petrolog4 User Interface

Petrolog4 can be used to perform six general types of calculations:

- Modelling Crystallisation,
- Modelling Reverse of Fractional Crystallisation,
- Estimation of Melt Liquidus Association,
- Modelling Melt Inclusions in Olivine,
- Calculating Normative Mineralogy, and
- Classification of chemical compositions.

Each calculation type can be selected by choosing the appropriate tab on the Main form of the software (Figure 1.1). Six tabs corresponding to the six calculation types above are called ‘Crystallisation’, ‘Reverse Crystallisation’, ‘Melt Liquidus Association’, ‘Olivine MI’, ‘Normative Mineralogy’ and ‘Classifications’.

Petrolog 4.2.5.1 Memory Usage: 1.888 Mb

File Export to MS Excel Tools Help

Crystallisation Reverse Crystallisation Melt Liquidus Association Olivine MI Normative Mineralogy Classifications

Models for phase-melt equilibrium:

Phase	Model	P	W	Tr
Olivine	Ford et al. 1983	Y		
Plagioclase	Press to Select			
Clinopyroxene	Press to Select			
Orthopyroxene	Press to Select			
Pigeonite	Press to Select			
Spinel	Press to Select			
Ilmenite	Press to Select			
Magnetite	Press to Select			
Sulfide	Press to Select			
Fluid	Press to Select			

☐ Force Pl-OI cotectic (for MORB and BABB only)

Extent of fractionation (%):

Phase	%fr
Olivine	100
Plagioclase	100
Clinopyroxene	100
Orthopyroxene	100
Pigeonite	100
Spinel	100
Ilmenite	100
Magnetite	100
Sulfide	100
Fluid	100

Oxidation state:
Calculations performed using:
[Oxygen Buffer: 'OFM'](#)
[Change Oxidation Models:](#)
Model for Fe: Borisov et al. 2018
Model for S: O'Neill & Mavrogenes 2022

Melt physical properties:
Density: [Lange & Carmichael 1987](#)
Viscosity: [Giordano & Dingwell 2003](#)

Calculation parameters:
Calculation step: 0.01 %
Define output frequency:
[Crystallisation step = 1.0 %](#)
A total of 1 output condition(s) chosen
Define conditions to stop calculations:
[Extent of crystallisation = 0 %](#)

Replenishment parameters:
[Recharge: Press to set...](#)
[Eruption: Press to set...](#)
[Trigger: Press to set...](#)

Starting melt composition:

SiO2	TiO2	Al2O3	Fe2O3	FeO	MnO	MgO	CaO	Na2O	K2O	P2O5	Cr2O3	H2O
50.00	1.00	15.00	0.00	9.00	0.10	10.00	12.00	2.50	0.20	0.10	0.10	0.00

☐ Fluid saturated ☐ Sulfide saturated
[Set volatile and trace elements](#)

PetrologDefault ☐ Calculate all analyses [Select another analysis](#)

Output to: Ptl_Otppt_*.csv D values: not set

Parameters: Program Default Set

[Start calculations](#) [Clear Results](#) Follow output: ☐ On

Figure 1.1 ‘Crystallisation’ tab of Petrolog4 interface with the Default set of parameters loaded.

Each tab window has three main parts: the top part (grey background) is used for setting the calculation parameters (Parameters Section); the middle part (white background) is used for recording calculation results (Output Section); and the optional bottom part (grey background) is used for recording non-critical

debugging messages and warnings (Debug Section). The Parameters Section has several entry fields and text boxes with white background (e.g., 'Calculation step' or 'Initial pressure'), in which parameter values can be typed in, and several settings in blue, which can be changed by clicking on them and choosing a different setting in a pop-up window.

When parameters are set, calculations are started by pressing the 'Start Calculations' button at the right-hand corner of the Parameters Section. The Output Section will list the set of parameters chosen for calculation and calculation results. Text in the Output Section can be highlighted and copied by simultaneously pressing 'Ctrl' and 'C', and then pasted into a text editor. (see Section 2 for details),

When calculation starts, the 'Start Calculations' button changes to the 'Interrupt Calculations' button, which can be used to abort the current run.

The program is loaded with the Program Default Set of parameters and a default starting composition ('PetrologDefault') and thus pressing the 'Start Calculations' button straight after the program is loaded would result in a default calculation.

Petrolog4.zip contains several recommended predefined sets of parameters for modelling crystallisation of several major geodynamic types of magmas such as mid-ocean ridge basalts and subduction-related magmas. These sets of parameters can also be downloaded from the Petrolog4 website.

Note: It is possible to save a set of parameters as the Default Set that would be loaded automatically every time Petrolog4 starts (see Section 4.2.1 of this Manual).

Figure 1.2. The main form of Petrolog4 with the content of the Tools Menu shown. Note that the Debug Section at the bottom of the Main Form is not displayed on this example as Debug output has been switched off by using the 'DebugOutput On/Off' item in the 'Tools' section of the Main Menu.

1.2. Petrolog4 Options

Petrolog4 options control some aspects of data input and output and allow the user to choose several other high-level options of program behaviour. Petrolog4 Options form is opened by selecting the 'Options' item in the 'Tools' section of the Main Menu (Figs. 1.2 and 1.3).

Note: Petrolog4 options are different from calculation parameters that control how calculations are performed (see Section 4 for a detailed description of calculation parameters).

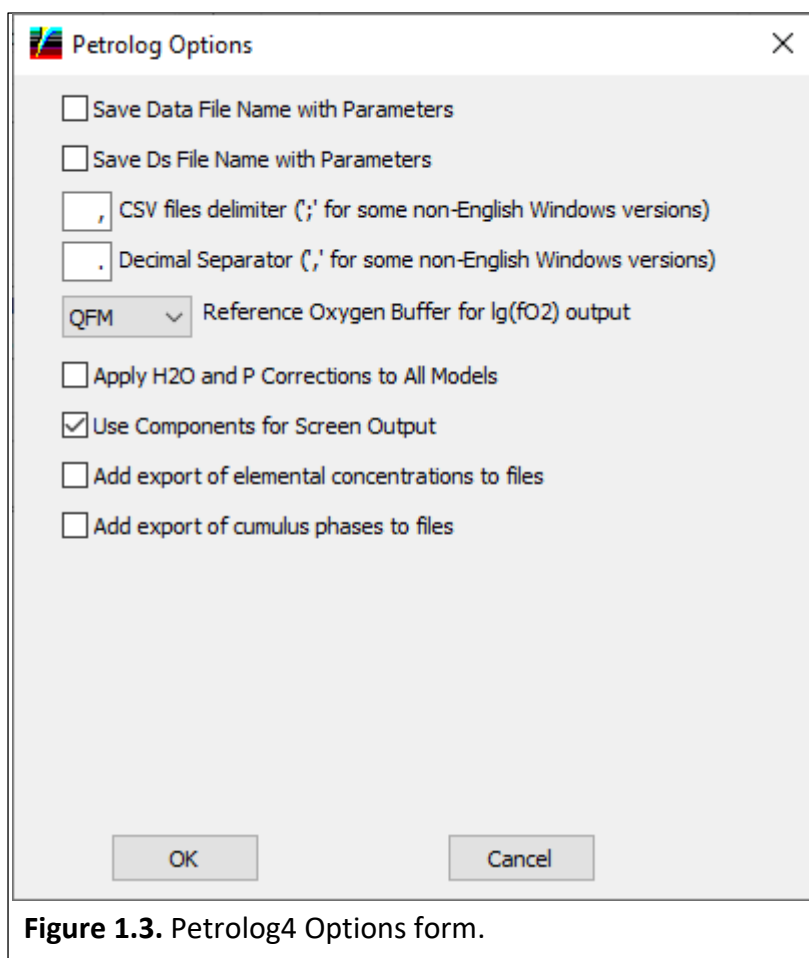


Figure 1.3. Petrolog4 Options form.

- 'Save Data File Name with Parameters' option defines whether a file with data (i.e., the starting compositions for calculations) is saved together with other calculation parameters (see Section 4.2). Default value is 'No'.

- 'Save Ds File Name with Parameters' option defines whether a file a user-defined set of distribution coefficients (D) for trace and volatile elements is saved together with other calculation parameters (see Sections 3 and 4.2). Default value is 'No'.

- 'CSV files delimiter' option defines how Petrolog4 saves the results of calculation to files (see Section 2.3). Default value is ','.

- 'Decimal Separator' option defines how Petrolog4 saves the results of calculation to files (see Section 2.3). Default value is '.'.

- 'Reference Oxygen Buffer for lg(fO₂) output' option defines how Petrolog4 saves the results of calculation to files (see Section 4.1.8). Default value is 'QFM'.

- 'Apply H₂O and P Corrections to All Models' option defines how the user-defined corrections to the calculated pseudo-liquidus temperatures for the effects of melt H₂O content and pressure are applied. Default value is 'No'. With the default setting, user defined corrections are only applied to mineral-melt equilibrium models that do not incorporate such effects. (see Sections 4.1.1.2 and 4.1.1.3). Advanced users may change this option to 'Yes' if they would like to introduce adjustments to specific models that incorporate such effects.

- 'Use Components for Screen Output' option defines whether concentrations of major and volatile elements are displayed using oxide or sulphide components or elements. (see Section 4.1.8). Default value is 'Yes'.

- 'Add export of elemental concentrations to files' option defines whether calculation output includes files with elemental concentrations in addition to files with component concentration (see Sections 2.2 and 4.1.8). Default value is 'No'.

- 'Add export of cumulus phases to files' option defines whether calculation output includes files with compositions of cumulus phases in addition to the combined composition of all cumulus phases (see Sections 2.2 and 4.1.8). Default value is 'No'.

2. Data Input and Output

2.1. Defining the Starting melt composition for calculations

The starting composition is set in the 'Starting Melt Composition' subsection of the Parameters Section (Fig. 1.1). Petrolog4 allows for the starting composition(s) to be entered manually or loaded from a file.

2.1.1. Manual entry of the starting composition.

When the program is loaded, the 'Starting melt composition' subsection of the Parameters Section contains the default starting composition 'PetrologDefault'. This composition can be edited directly within this section. The concentrations of major elements and H₂O are in wt.% oxides.

Trace and volatile element contents are set and/or edited by clicking on 'Set volatile and trace elements' label, which opens the 'Volatile and Trace Elements' pop-up window (Fig 2.1).

Element	Value
H2O_wt%	0
CO2_ppm	0
S_ppm	0
SO3_ppm	0
Cl_ppm	0
Li_ppm	0
B_ppm	0
Be_ppm	0
Sc_ppm	0
V_ppm	0
Co_ppm	0
Ni_ppm	0
Cu_ppm	0
Zn_ppm	0
Ga_ppm	0
Rb_ppm	0
Sr_ppm	0
Y_ppm	0
Zr_ppm	0
Nb_ppm	0
Ru_ppm	0
Rh_ppm	0
Pd_ppm	0
Cs_ppm	0
Ba_ppm	0
La_ppm	0
Ce_ppm	0
Pr_ppm	0
Nd_ppm	0
Sm_ppm	0
Eu_ppm	0
Gd_ppm	0
Tb_ppm	0
Dy_ppm	0

Set all to 0 OK Cancel

Figure 2.1. Window for setting volatile and trace element contents.

The concentrations of volatile and trace elements of interest are entered into the column 'Value' in wt. ppm (all but H₂O). All elements that have concentrations above zero will be included in calculations. To reset all concentration values to zero press 'Set all to 0' button. Pressing the 'Cancel' button will close the form without applying any changes that were made.

Note: Sulphur can be entered as S or SO₃ or both. When multiple forms of S are present in the starting composition, the total elemental S content is calculated by summing sulphur entered in different forms. The oxidation state of sulphur is determined during calculations based on the magma oxidation state (see Section 4.1.5). Reduced S²⁻ is coupled to Fe²⁺ in the melt.

Note: If contents of at least one volatile / trace element are set to a non-0 value, a star (*) appears next to the 'Set volatile and trace elements' label in the 'Starting melt composition' subsection (Fig. 2.2).

2.1.2. Loading starting composition(s) from file.

The starting composition(s) can also be loaded from a file by using the 'Open data file' option in the 'File' menu (Fig. 2.2).

Note: When a file is loaded, its name and full path are displayed at the top of the Petrolog4 Main form (Fig. 2.2).

The data file should contain analyses stored as rows with the first row containing element names. The program can read delimited text files that use 'tabs', blank spaces, commas or semicolons as delimiters. The recognised extensions for file names are '.txt', '.dat' and '.csv'.

Note: The order of elements in the file is not prescribed. Petrolog4 identifies elements by analysing the first row of the data file.

The following abbreviations should be used (not case sensitive): SiO₂, TiO₂, Al₂O₃, Fe₂O₃, FeO, FeO* or FeOt, MnO, MgO, CaO, Na₂O, K₂O, P₂O₅, Cr₂O₃, H₂O, CO₂, S, SO₂, SO₃, Cl, F, B, Be, Sc, V, Co, Ni, Cu, Zn, Ga, Rb, Sr, Y, Zr, Nb, Ru, Rh, Pd, Cs, Ba, La, Ce, Pr, Nd, Sm, Eu, Gd, Tb, Dy, Ho, Er, Tm, Yb, Lu, Hf, Ta, Re, Os, Ir, Pt, Pb, Th, U. Concentrations of major element oxides and H₂O should be supplied in wt.% and for all other elements in wt. ppm. Names of all elements supplied as wt. ppm can be followed by '_ppm'; the name for H₂O can be followed by '_wt%'. Petrolog4 can also read melt compositions from its output files (section 2.2). At least 4 major elements SiO₂, FeO or Fe₂O₃, MgO and CaO must be present at above 0 concentrations to make a valid data

file. The column containing analysis identifiers can be called either 'Name' or 'Sample' or 'Number' or 'Analysis'.

Note: The data file can also contain other columns as described later in this Manual (Sections 4.1.3 and 4.1.10).

Note: When both FeO and the total Fe as FeO (FeO* or FeOt) columns are present in the file, the user will be asked to choose whether to load data from the Fe₂O₃ and FeO columns and ignore the total Fe values, or to load the total Fe as FeO and ignore the FeO and Fe₂O₃ values.

Note: Sulphur can be entered as either S, or SO₂, or SO₃ in any combination. When multiple forms of S are present in the starting composition, the total elemental S content is calculated by summing sulphur entered in different forms. The oxidation state of sulphur is determined during calculations based on the magma oxidation state (see Section 4.1.5). Reduced S²⁻ is coupled to Fe²⁺ in the melt.

Note: The starting composition in the 'Starting melt composition' subsection of the Main form does not change during calculations and can be used in subsequent calculations if required.

Petrolog 4.2.2 Input from: C:\Programs\Delphi\Petrolog4\Manual\Current_data_File.csv Memory Usage: 1.899 Mb

File Export to MS Excel Tools Help

Open Data File
File for output...
Save Parameters
Load Parameters
Save Parameters as the Default Set
Load the Default Set of Parameters
Exit...

Open Data File
File for output...
Save Parameters
Load Parameters
Save Parameters as the Default Set
Load the Default Set of Parameters
Exit...

Force Pl-OI cotectic (for MORB and BABB only)

Extent of fractionation (%):

Phase	%fr
Olivine	100
Plagioclase	100
Clinopyroxene	100
Orthopyroxene	100
Pigeonite	100
Spinel	100
Ilmenite	100
Magnetite	100
Sulfide	100
Fluid	100

Oxidation state:
Calculations performed using:
Oxygen Buffer: QFM
Change Oxidation Models:
Model for Fe: Borisov et al 2018
Model for S: O'Neill & Mavrogenes 2022

Melt physical properties:
Density: Lange & Carmichael 1987
Viscosity: Giordano & Dingwell 2003

Calculation parameters:
Calculation step: 0.01 %
Define output frequency:
Crystallisation step = 1.0 %
A total of 1 output condition(s) chosen
Define conditions to stop calculations:
Extent of crystallisation = 0 %

Saturation Models:
Change Saturation Models:
Sulfide : Smythe et al. 2017
Fluid : Iacono-Marziano et al 2012
Sulfate : Zajacz & Tsay 2019
Apatite : Tollari et al. 2006
Zircon : Crisp & Berry 2022

Pressure:
Initial P (kbar): 0.001
Set Pressure behaviour:
Keep constant

Replenishment parameters:
Recharge: Press to set...
Eruption: Press to set...
Trigger: Press to set...

Starting melt composition:

SiO ₂	TiO ₂	Al ₂ O ₃	Fe ₂ O ₃	FeO	MnO	MgO	CaO	Na ₂ O	K ₂ O	P ₂ O ₅	Cr ₂ O ₃	H ₂ O
48.00	1.00	14.00	0.50	9.00	0.16	7.00	9.00	2.00	0.20	0.22	0.08	0.00

Analysis1

Calculate all analyses

Select another analysis

Set volatile and trace elements*

Output to: Ptl_Otpt_*.csv
Parameters: Program Default Set modified

D values: not set

Start calculations Clear Results Follow output: On

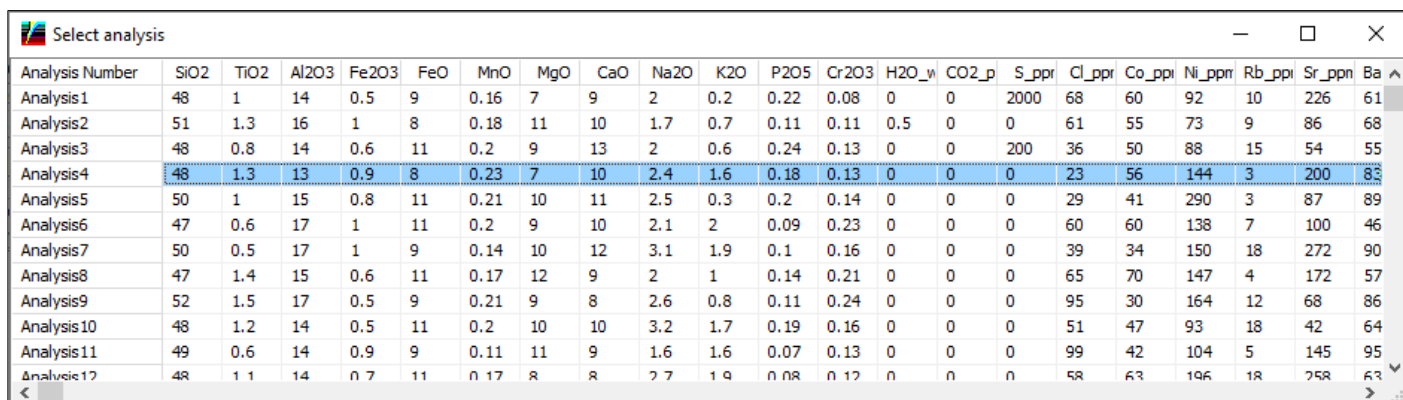
C:\Programs\Delphi\Petrolog4\Manual\Current_data_File.csv loaded successfully

Figure 2.2. The Main form of Petrolog4 with the content of the File Menu shown. The name of the loaded data file with the starting compositions is displayed at the top of the form. The name of the loaded file with calculations parameters (if loaded) is displayed above the Output window on the left side of the form. The name of the file with distribution coefficients for trace and volatile elements (D values), if loaded, is displayed above the Output window in the centre of the form. The name of the file for saving the result is displayed above the Output window on the left side of the form.

When a file is loaded, the first analysis in the file is displayed in the 'Starting melt composition' subsection. The values in this analysis can be edited in Petrolog4 without affecting the data file stored on disk. When the

'Start calculations' button is pressed, the calculations will start using the composition displayed in the 'Starting melt composition' subsection.

If the data file contains more than one analysis, it is possible to choose another analysis by clicking on the 'Select another analysis' label in the 'Starting melt composition' subsection. In the pop-up window that appears (Fig. 2.3), *double-click* on the required analysis to choose it (click anywhere on the concentration values, not on the 'Analysis Number' column). This will close the window and return to the Main form. The concentration values for the chosen analysis will appear in the 'Starting melt composition' subsection of the Main form. To close the 'Select analysis' window without choosing an analysis, click on the cross in the top right corner.



Analysis Number	SiO2	TiO2	Al2O3	Fe2O3	FeO	MnO	MgO	CaO	Na2O	K2O	P2O5	Cr2O3	H2O_w	CO2_p	S_ppm	Cl_ppm	Co_ppm	Ni_ppm	Rb_ppm	Sr_ppm	Ba
Analysis1	48	1	14	0.5	9	0.16	7	9	2	0.2	0.22	0.08	0	0	2000	68	60	92	10	226	61
Analysis2	51	1.3	16	1	8	0.18	11	10	1.7	0.7	0.11	0.11	0.5	0	0	61	55	73	9	86	68
Analysis3	48	0.8	14	0.6	11	0.2	9	13	2	0.6	0.24	0.13	0	0	200	36	50	88	15	54	55
Analysis4	48	1.3	13	0.9	8	0.23	7	10	2.4	1.6	0.18	0.13	0	0	0	23	56	144	3	200	83
Analysis5	50	1	15	0.8	11	0.21	10	11	2.5	0.3	0.2	0.14	0	0	0	29	41	290	3	87	89
Analysis6	47	0.6	17	1	11	0.2	9	10	2.1	2	0.09	0.23	0	0	0	60	60	138	7	100	46
Analysis7	50	0.5	17	1	9	0.14	10	12	3.1	1.9	0.1	0.16	0	0	0	39	34	150	18	272	90
Analysis8	47	1.4	15	0.6	11	0.17	12	9	2	1	0.14	0.21	0	0	0	65	70	147	4	172	57
Analysis9	52	1.5	17	0.5	9	0.21	9	8	2.6	0.8	0.11	0.24	0	0	0	95	30	164	12	68	86
Analysis10	48	1.2	14	0.5	11	0.2	10	10	3.2	1.7	0.19	0.16	0	0	0	51	47	93	18	42	64
Analysis11	49	0.6	14	0.9	9	0.11	11	9	1.6	1.6	0.07	0.13	0	0	0	99	42	104	5	145	95
Analysis12	48	1.1	14	0.7	11	0.17	8	8	2.7	1.9	0.08	0.12	0	0	0	58	63	106	18	258	63

Figure 2.3. Window for selecting an analysis from the imported datafile.

2.1.2.1. Calculating multiple analyses from the loaded data file

Petrolog4 offers an option of calculating all analyses in the data file using the same set of calculation parameters. The data file can also contain columns that store parameters for stopping calculations for each analysis (see Section 4.1.10 for details).

When a data file is loaded, the 'Calculate all analyses' check box becomes active (Fig. 2.2) if there is more than one analysis in the file.

Note: When the 'Calculate all analyses' box is checked, Petrolog4 ignores the composition in the 'Starting melt composition' subsection, and instead reads analyses consequently from the loaded data file.

2.2. Saving the results of calculations to a file

Petrolog4 offers three options for saving calculation results for future use.

I. During calculations, Petrolog4 continuously prints the state of the system into the Output Section of the Main form (Fig. 1.1). This output can be highlighted within the Output Section by first clicking inside the section and pressing Ctrl+A, and then copied (Ctrl+C) to the clipboard and pasted into a text editor.

II. By default, Petrolog4 always saves the results into several 'comma-separated values' files named 'Ptl_Otpt_*.csv'. The output file name currently in use is displayed above the Output window on the left side of the Main form (Figs. 1.1, 2.2). The number of files created by Petrolog4, and their structure, depend on the chosen calculation option and will be described later in this Manual.

Note: Output files saved during modelling crystallisation calculations have 'FRAC' added to their name (i.e., 'Ptl_Otpt_FRAC_*.csv'); output files saved during modelling reverse of fractional crystallisation calculations have 'REV' added to their name; output files saved during estimation of melt liquidus association calculations have 'MLA' added to their name; output files saved during modelling melt inclusions in olivine have either 'IRL' or 'PIC' or 'PCR' added to their name, depending on the chosen type of calculations.

After the calculations are completed, the saved files can either be opened manually (not recommended) or can be imported into Excel (recommended) by using the 'Export to MS Excel' section of the Main Menu (Figs. 1.1, 2.2). The latter creates an Excel workbook with several worksheets containing all the details of the calculation. To export the latest results, use 'Results of the last calculation' option.

Note: When the default output file name is used, the output files from the last calculation will be overridden when a new calculation of the same type starts. If you would like to keep the results of the previous calculation, export them to Excel prior to starting a new calculation.

III. Petrolog4 can save the output into .csv files with a user-specified name.

To specify the output file name, use the 'File for output...' option in the 'File' section of the Main Menu on the Main form (Fig. 2.2). Type in the desired file name into the 'File name:' field on the 'Save As' dialog form that opens, choose the folder for saving the file, and press the 'Save' button. Do not provide an extension for the file name as it will be ignored.

These files can be opened or loaded in Excel in a similar way as described for option II. You can choose either 'Results of previous calculations' or 'Results of the last calculation'. When exporting results of a previous calculation, a dialog window pops-up where the user should select the file to open, as explained for each calculation type later in this Manual.

Note: If the user-specified file name is not changed before starting a new calculation of the same type, results of the previous calculation will be overwritten at the start of the new calculation.

2.3. Reading data files and saving the results of calculations when using non-English language versions of Windows

Petrolog4 allows the user to choose the decimal separator and the delimiter for the comma-delimited-values text files (*.csv). The default settings are '.' for the decimal separator and ',' for the *.csv delimiter, that are default settings for English language versions of Windows. The user can change the separator to ';' and the delimiter to ',' in the Petrolog Options form (see Section 1.2) that can be displayed by choosing the 'Options' item in the 'Tools' section of the Main Menu.

Note: These settings only affect the format of files read and written by Petrolog4. They have no effect on the display of numbers within the software.

3. Defining and storing sets of values of distribution coefficients (D) for trace and volatile elements

In general, distribution coefficients (D) are defined as $D_{\text{phase}}^i = C_{\text{phase}}^i / C_{\text{melt}}^i$, where 'Cⁱ' are concentrations of element 'i' in a phase (e.g., plagioclase, fluid, sulphide melt, etc.) and in silicate melt.

Petrolog4 provides three approaches to handling distribution coefficients. To define D values, use the 'Set D values' option in the 'Tools' menu (Fig. 1.2). A window 'Set D Values' will open (Fig. 3.1).

Note: Petrolog4 assigns a charge of +4 to the oxidised sulphur in the fluid. Thus, the D value for oxidised sulphur between the fluid and silicate melt is defined as $C_{\text{fluid}}^{\text{SO}_2} / C_{\text{melt}}^{\text{SO}_3}$. In all other phases, the charge of oxidised sulphur is +6.

Element	Olv	Plg	Cpx	Opx	Piq	Spl	Ilm	Mgt	Slf	Flid	Sft	Qtz	Ort	Nph
H2O	0	0	0	0	0	0	0	0	0	0	0	0	0	0
CO2	0	0	0	0	0	0	0	0	0	0	0	0	0	0
S2-	0	0	0	0	0	0	0	0	0	Ding2023	0	0	0	0
S+	0	0	0	0	0	0	0	0	0	Ding2023	0	0	0	0
Cl	0	0	0	0	0	0	0	0	0	0	0	0	0	0
O	0	0	0	0	0	0	0	0	KiWd2015	0	0	0	0	0
CH4	0	0	0	0	0	0	0	0	0	0	0	0	0	0
F	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Li	0.02	0	0	0	0	0	0	0	0	0	0	0	0	0
B	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Be	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Sc	0	0	0	0	0	0	0	0	0	0	0	0	0	0
V	0	0	0	0	0	0	0	0	KiWd2015	0	0	0	0	0
Co	Beatt91	0	0.2	0.8	0.8	0	0	0	KiWd2015	0	0	0	0	0
Ni	Herzb02	0	1	1.5	1.2	0	0	0	KiWd2015	0	0	0	0	0
Cu	0	0	0	0	0	0	0	0	KiWd2015	0	0	0	0	0
Zn	0	0	0	0	0	0	0	0	KiWd2015	0	0	0	0	0
Ga	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Rb	0.001	0.1	0.05	0.02	0.03	0	0	0	0	0.2	0	0	2	0
Sr	0.01	Bl_Wo91	0.07	0.05	0.05	0	0	0	0	0.1	0	0	0	0
Y	0	0	Wo_Bi97	0	0	0	0	0	0	0	0	0	0	0
Zr	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Nb	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Ru	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Rd	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Pd	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Cs	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Ba	0	Bl_Wo91	0.03	0.015	0.02	0	0	0	0	0.3	1.5	0	0	0
La	0	0	Wo_Bi97	0	0	0	0	0	0	0	0	0	0	0

Figure 3.1. Form for defining D values to be used in calculations. Blue background identifies element / phase pairs for which models for D values are available (see approach III). When clicking on such a cell, a popup window will appear in the middle of the form when the user clicks on the cell corresponding to such an element, as shown for Sr in plagioclase. See text for details.

Note: Although this form lists methane (CH₄), the current version of Petrolog4 does not incorporate methane and methane row is disabled on the form.

Approach I. Some of the phase-melt equilibrium models incorporate some trace and volatile elements. When such models are chosen for calculations, by default the concentrations of trace and volatile elements incorporated in the model will be calculated following the approach used in the model. When such models are chosen, their names will be displayed in the corresponding cells on the form (e.g., on Fig. 3.1. Herzberg and O'Hara, 2002 for olivine melt-equilibrium incorporates Ni; Kiseeva et al., 2015 for sulphide-melt – silicate-melt equilibrium incorporates V, Co, Ni, Cu, Zn, Pb; thus 'Herzb02' is displayed in the Ni cell for olivine and 'KiWd2015' is displayed for the V, Co, Ni, Cu, Zn cells for sulphide).

Approach II. One can set a constant D value, which is then used in the calculation(s). Constant D values for any phase/element pair can be set by entering them into the corresponding cells (Fig. 3.1). The entered D values must be calculated using weight units of concentration.

Note: If desired, the displayed model names can be overwritten by a constant D value by entering the value into the corresponding cell instead of the shown name.

Note: Oxygen is considered a major element in all phases but sulphide, and thus a D value for oxygen can only be set for sulphide.

Note: Although it is possible to set D values for H₂O and CO₂ in the fluid phase, if the chosen model for the fluid phase incorporates either of these elements they would be considered as major elements for the fluid phase, and thus the entered D values will be ignored (the concentrations will be calculated by the chosen model of fluid - silicate melt equilibrium).

Note: Reduced sulphur is considered a major element in sulphide, and thus a D value for reduced sulphur can be set for all phases but sulphide.

Note: Oxidised sulphur is considered a major element in sulphate, and thus a D value for oxidised sulphur can be set for all phases but sulphate.

Note: Zirconium is considered a major element in zircon, and thus a D value for Zr can be set for all phases but zircon.

Approach III. Petrolog4 allows for using models that define D values for an element in a phase as a function of various parameters, such as melt composition, temperature, phase composition, etc. D models available in the current version of Petrolog4 are listed in Appendix 1, and the corresponding cells are highlighted by blue background on the 'Set D Values' form.

If D models are available for an element in a phase, a pop-up window will appear when clicking on the cell for that element/phase (Fig. 3.1). The pop-up window will display all available models for the element in the phase. All elements available in the model are listed (e.g., Ba and Sr are available in the Blundy and Wood, 1991 model for plagioclase, Fig. 3.1). Clicking on the list of elements (not the name of the model) will apply the model to the selected element. If the 'Set for all elements' checkbox is ticked before selecting a model, the model will be applied for all elements that are part of this model, not just the one that was clicked on the form. If required, D values for individual elements in the list can be later set to constant values by entering the D value into the 'Set D Value:' box and pressing the 'Close panel' button. This will not affect the application of the chosen model to the remaining elements in the list.

Note: The pop-up window only appears when clicking on an element for which a D model is available. The pop-up window disappears after clicking on a cell for an element for which no D models are available in Petrolog4.

To save the chosen set of D values and models, press the 'Save this set of Ds' button. In the dialog form that appears, enter a file name and press Save.

Note: Petrolog4 assigns .PtIDSet extension to files with D values.

To load a saved set of D values, press the 'Load a set of Ds from file' button, choose the file in the dialog window, and press Open.

To finish editing D values, close the form by pressing the 'Ok' button. To close the form without applying any of the changes, press the 'Cancel' button.

4. Modelling crystallisation

To model crystallisation, chose 'Crystallisation' tab of the Main form (Figs. 1.1, 1.2, 2.2).

4.1. Setting calculation parameters

The following calculation parameters can be set before starting calculations:

- set of phases involved in calculations;
- phase-melt equilibrium model for each phase;
- extent of fractionation for each phase;
- melt oxidation state;
- fluid, sulphur, zircon and apatite saturation models;
- forced fluid and/or sulphide saturation
- pressure;
- melt density and viscosity models;
- calculation step;
- conditions for stopping calculations;
- conditions for the output of results during calculation
- conditions for modelling replenishment.

These are described in detail below.

Note: Petrolog4.zip file contains recommended predefined sets of parameters for modelling crystallisation of several major geodynamic types of magmas such as mid-ocean ridge basalts and subduction-related magmas. These sets of parameters can also be downloaded from the Petrolog4 website.

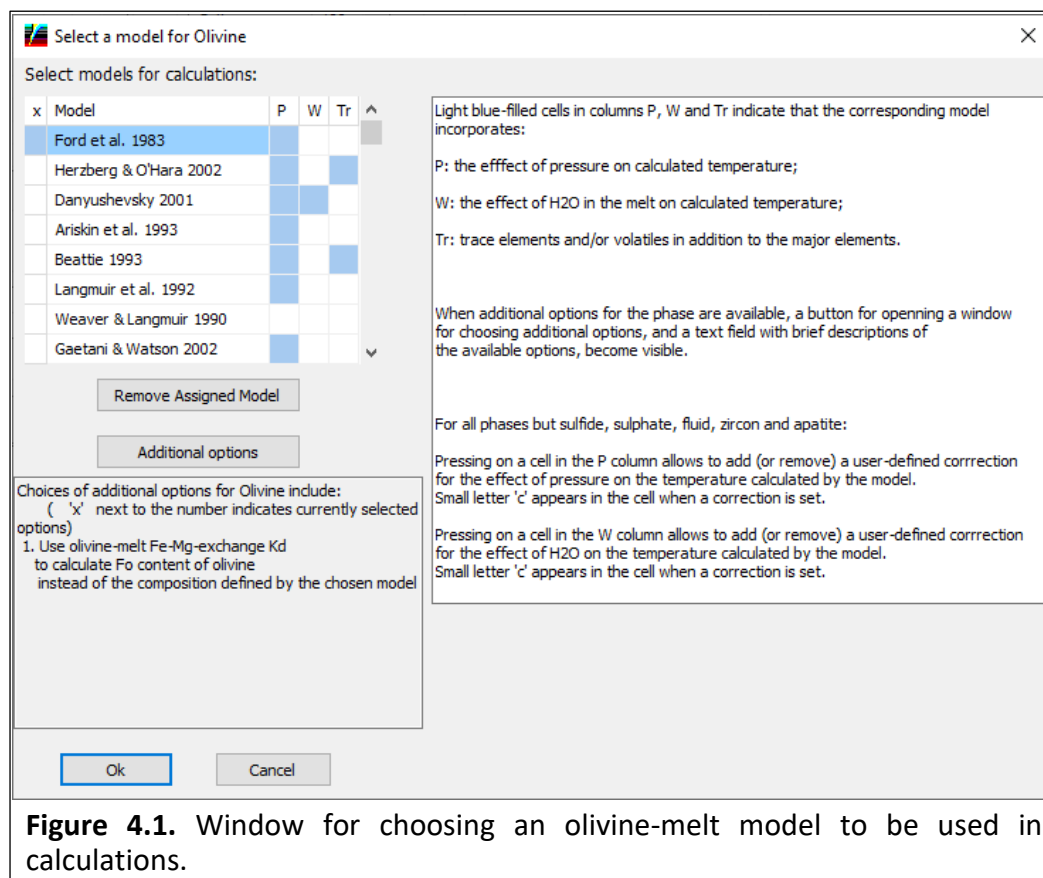
4.1.1. Choosing phases and phase-melt equilibrium models

Phases and models are chosen in the 'Models for phase-melt equilibrium' subsection of the Parameters Section (Figs. 1.1, 1.2).

When 'Press to Select' is written in the 'Model' field next to a phase name when 'Start calculations' button is pressed, this phase will not be included in calculations. If a model abbreviation is written next to a phase name (e.g., Ford et al., 1983 next to Olivine on Fig. 1.1), the phase will be included in calculations.

Note: Selecting a phase for calculations does not guarantee that it will appear on the liquidus during calculations. Petrolog4 algorithm determines the order of crystallisation based on the chosen parameters.

To choose a model for a phase, click on the 'Model' field for that phase (Figs. 1.1, 1.2). A pop-up window with a list of available models for this phase will appear (Fig. 4.1).



This window contains a table with 4 columns. Text box on the right provides a brief explanation on how to use the form and interpret the information shown on the form.

Column 'Model' lists model abbreviations. Column 'P' indicates whether a model incorporates the effect of pressure on the phase-melt equilibrium (the cell is coloured light blue), or alternatively it is designed for the atmospheric pressure only (the cell has white background). Column 'W' indicates whether a model incorporates the

effect of H₂O on phase -melt equilibrium (the cell is coloured light blue), or alternatively it is designed for anhydrous conditions only (the cell has white background). Column 'Tr' indicates whether a model incorporates any trace or volatile elements. If the 'Tr' cell for a model is coloured light blue, the model incorporates some of those elements. Blue rectangle to the left of the Ford et al. (1983) cell indicates that this model is currently chosen for calculations.

Clicking on the name of a different model will change selection to that model.

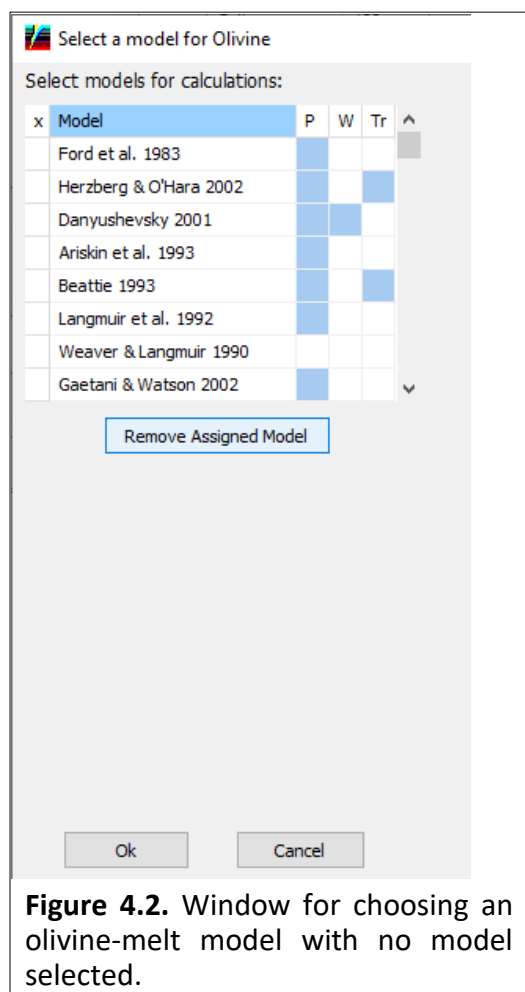


Figure 4.2. Window for choosing an olivine-melt model with no model selected.

Clicking on the 'Remove Assigned Model' button will deselect the selected model and not select any other model (Fig. 4.2). When no model is assigned, the 'Additional Options' button is not shown even when such options are available for the phase. Clicking on the 'Ok' button when no model is selected will result in 'Press to Select' showing next to the phase in the 'Models for phase-melt equilibrium' subsection of the Main form (Figs. 1.1, 1.2, 2.2).

Note: The available models for sulphide, sulphate, zircon, apatite and fluid calculate the compositions of these phases for the given pressure, temperature and melt composition. Thus, including these models in calculations requires choosing at least one silicate or oxide mineral-melt model to define melt liquidus temperature.

Note: Before starting calculations: 1) when either H₂O or CO₂ are present in the starting composition, the user must choose a model for fluid-melt equilibrium; 2) when S is present in the starting composition, the user must choose a sulphide melt – silicate melt and a sulphate melt – silicate melt equilibrium model.

Note: When selecting a fluid-melt model, a text field will appear above the OK button that displays the pressure range for the chosen model.

Clicking on the 'Cancel' button on this form will close the form without applying any of the changes made.

Once the 'Select a model' form is closed, to set a model for another phase, click on the 'Model' field for that phase in the 'Models for phase-melt equilibrium' subsection of the Parameters Section (Figs. 1.1, 1.2, 2.2).

4.1.1.1. Additional options for calculating phase compositions

In the current version, additional options are available for olivine and plagioclase. When options are available, the 'Additional options' button and a text field with brief descriptions of the available options are displayed on the form (Fig. 4.1). When an additional option is chosen, 'x' appears next to its description in the text field. Clicking on the 'Additional options' button opens the Additional Options form (Fig. 4.3).

4.1.1.1a. Additional options for olivine

When choosing a model for olivine-melt equilibrium, the 'Use olivine-melt Fe-Mg-exchange Kd to calculate olivine Fo content' check box on the Additional Options form can be used to set an olivine-melt Fe-Mg exchange Kd value for calculation of olivine composition. This calculated composition will be used instead of the composition calculated by the selected olivine-melt model.

Note: When calculating olivine compositions using a Kd value, the olivine-melt equilibrium model chosen in the 'Select a model for Olivine' window (Fig. 4.1) is used for calculating olivine crystallisation temperature.

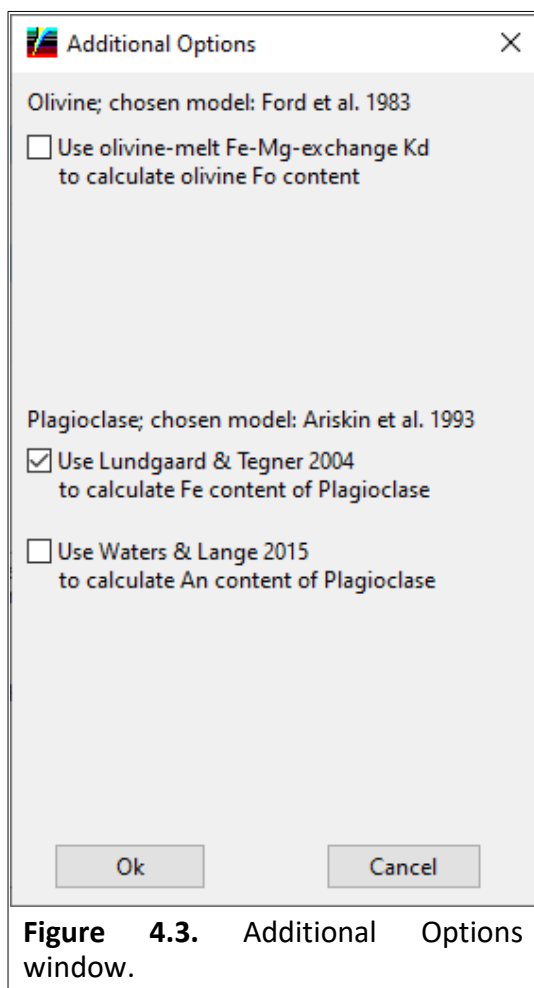


Figure 4.3. Additional Options window.

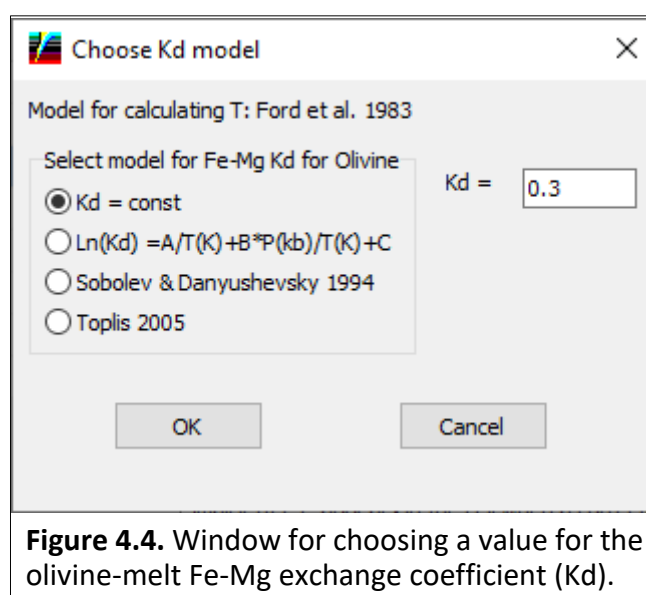


Figure 4.4. Window for choosing a value for the olivine-melt Fe-Mg exchange coefficient (Kd).

When the box is switched to 'checked', a pop-up window appears that is used to determine how the Kd values are determined (Fig. 4.4). Four options are available for calculating Kd values:

(1) 'Kd = const': When this option is chosen, a Kd value must be entered in the box to the right, that will be used in calculations.

(2) ' $\ln(Kd) = A/T(K)+B*P(kbar)/T(K)+C$ ': When this option is chosen, values for coefficients A, B and C must be provided. The default values correspond to a Kd value of 0.3.

(3) 'Sobolev & Danyushevsky 1994': When this option is chosen,

Kd values will be calculated following the method described in the Appendix 1 of Sobolev and Danyushevsky (1994).

(4) 'Toplis 2005': When this option is chosen, Kd values will be calculated using the method of Toplis (2005).

Pressing the 'Cancel' button will close the form without applying any of the changes made.

To deselect the Kd option, uncheck the 'Use olivine-melt Fe-Mg-exchange Kd to calculate olivine Fo content' box by clicking on it when it is checked.

4.1.1.1b. Additional options for plagioclase

When selecting a plagioclase-melt equilibrium model, the user is given a choice of using the Waters and Lange (2015) model to calculate plagioclase anorthite content, and Lundgaard and Tegner (2004) model for ferric and ferrous iron equilibrium between plagioclase and melt (Fig. 4.3).

When the Waters and Lange (2015) model an option is selected (the checkbox on the form is checked), the anorthite content in plagioclase will be calculated by using this model, overriding the plagioclase composition calculated by the chosen plagioclase-melt equilibrium model. The chosen plagioclase-melt equilibrium model will be used for calculating plagioclase crystallisation temperature, but not the composition.

Note: The Waters and Lange (2015) model is not applicable to all melt compositions and may fail to calculate anorthite content of plagioclase. In such cases, calculation of plagioclase compositions will revert to the chosen plagioclase-melt equilibrium model, and the option to use the Waters and Lange (2015) model will be deselected.

When the Lundgaard and Tegner (2004) model is selected (the checkbox on the form is checked), the Fe content in plagioclase will be calculated by using this model, overriding the Fe content calculated by the chosen plagioclase-melt equilibrium model (if the chosen model incorporates Fe content in plagioclase).

This option is provided as most available plagioclase-melt models do not calculate Fe content in plagioclase.

4.1.1.2. Setting a pressure correction to the temperature calculated by the chosen model

Petrolog4 offers an option to introduce a linear correction for the effect of pressure on the pseudo-liquidus temperature calculated by a model. A separate correction value can be set for each mineral involved in calculations. To set a correction, click on the 'P' cell next to the chosen model (Fig. 4.1). This opens a pop-up window where a correction value in degrees/kbar can be set (Fig. 4.5).

The window is titled "Pressure correction for the current model". It shows the model "Ariskin et al. 1993" is selected. There is a checkbox "Correct for Pressure" which is checked, and a text input field next to it containing "9.5" with the unit "°C / kbar". Below this is an unchecked checkbox "Use Petrolog default" and a button "Set Default for all Minerals". At the bottom are "Ok" and "Cancel" buttons.

Figure 4.5. Window for setting a correction for the effect of pressure on the calculated liquidus temperature.

The window is titled "Select a model for Plagioclase". It contains a table with columns "Model", "P", "W", and "Tr". The "Ariskin Barmina 1990" model is selected, and a red 'c' is visible in the "P" column. Below the table is a "Remove Assigned Model" button and an "Additional options" button. At the bottom are "Ok" and "Cancel" buttons.

x	Model	P	W	Tr
	Pletchov & Gerya 1998			
	Ariskin et al. 1993			
	Langmuir et al. 1992			
	Ariskin Barmina 1990	c		
	Weaver & Langmuir 1990			
	Nielsen 1985			
	Nielsen & Dungan 1983			
	Drake 1976			

Choices of additional options for Plagioclase include:
 ('x' next to the number indicates currently selected options)
 x1. Use Lundgaard & Tegner (2004) to calculate Fe content in Plagioclase instead of the Fe contents defined by the chosen model
 2. Use Waters & Lange (2015) to calculate Anorthite content in Plagioclase instead of the composition defined by the chosen model

Figure 4.6. Window for choosing a model for plagioclase-melt equilibrium; 'c' in column 'P' indicating that a pressure correction is set.

The user can set a value for the correction, or chose to use the Petrolog4 default correction value, by clicking on 'Use Petrolog Default' (See Appendix 1 for Petrolog Default corrections).

Pressing the 'Cancel' button will close the form without applying any changes.

When correction is set, a small letter 'c' on red background appears in the 'P' cell next to the chosen model (Fig. 4.6).

Note: Since sulphide melt, sulphate, fluid, zircon and apatite models do not calculate crystallisation temperatures, a pressure correction cannot be set for these phases.

Note: If the 'Ok' button is clicked when the correction value is 0, no correction is applied, even if the 'Correct for Pressure' checkbox is checked.

Note: If a chosen model incorporates the effect of pressure (e.g., models of Langmuir et al. 1992 and Ariskin at al. 1993 on Fig. 4.6), then the option 'Apply H₂O and P Corrections to All Models' (Fig.1.3) defines whether the correction will apply. When the option is not selected (recommended), the correction will only apply to models that do not incorporate pressure.

Note: Once chosen, a correction applies to all models, i.e., if the phase-melt model is changed after the correction is set, the correction will be transferred to the new model. To remove the correction, open the 'Pressure correction' window again (Fig. 4.5) and uncheck the 'Correct for Pressure' box. The small letter 'c' in the 'P' cell will disappear returning the form to its original state.

Note: Setting a user-defined correction for the effect of pressure on the pseudo-liquidus temperature, does not affect the mineral composition that the chosen model calculates.

4.1.1.3. Setting an H₂O correction to the temperature calculated by the chosen model

As only a few models available in Petrolog4 incorporate the effect of melt H₂O content on pseudo-liquidus temperature and/or composition of crystallizing phases (e.g., Plechov and Gerya,

1998; Danyushevsky, 2001; Putirka, 2005; Plechov et al. 2023), Petrolog4 allows the user to introduce corrections to the 'anhydrous' models for the effect of H₂O on calculated temperatures, to enable calculations under hydrous conditions using models developed for anhydrous conditions.

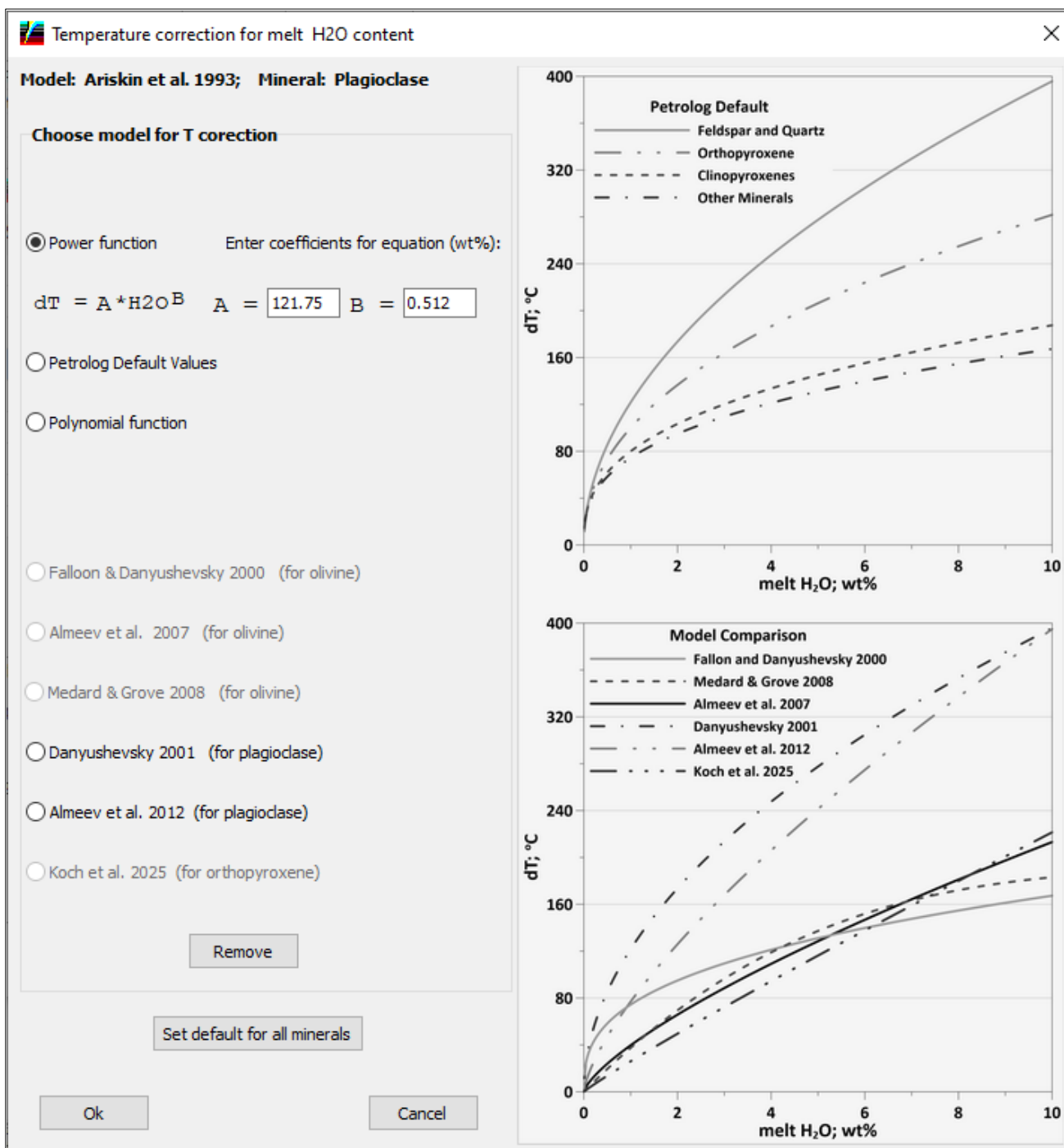


Figure 4.7. Window for setting a correction for the effect of H₂O on liquidus temperature of plagioclase.

To set a correction, click on the 'W' cell next to the chosen model (Figs. 4.1, 4.6). This opens a pop-up window 'Temperature correction for melt H₂O content' (Fig. 4.7) which is used to set the correction.

Note: Similarly to the pressure correction described above, applying an H₂O correction to the calculated temperature does not affect the calculated phase compositions. Also similarly to the pressure correction, an H₂O correction cannot be set for sulphide melt and fluid models.

Note: Similarly to the pressure correction described above, if a chosen model incorporates the effect of H₂O, then the option 'Apply H₂O and P Corrections to All Models' (Fig. 2.4) defines whether the correction will apply. When is not selected (recommended), the correction will apply to models that do not incorporate the effect of H₂O.

Petrolog4 offers several options for setting an H₂O correction: user defined power or polynomial functions, Petrolog4 default corrections, and published models for setting H₂O correction that are currently available for olivine, plagioclase and orthopyroxene. Petrolog4 default corrections are plotted on the top graph on the

form. A comparison between published models is plotted on the bottom plot on the form. The list of available models for H₂O corrections and parameters for Petrolog4 default corrections are presented in Appendix 1.

A polynomial correction can be set in a form: $dT (^{\circ}C) = A * (H_2O \text{ wt.}\%)^3 + B * (H_2O \text{ wt.}\%)^2 + C * (H_2O \text{ wt.}\%)$.

Note: if desired, a linear correction can be set by using either power or polynomial corrections and setting B to 1 for the former or setting A and B to 0 for the latter.

When a correction is set, small letter 'c' on red background appears in the 'W' cell next to the chosen model (Fig. 4.8).

Note: Once chosen, a correction, applies to all models, i.e., if the phase-melt model is changed after the correction is set, the correction will be transferred to the new model. To remove the correction, open the 'Temperature correction for melt H₂O content' window again (Fig. 4.7) and press 'Remove' button. The small letter 'c' in the 'W' cell will disappear returning the form to its original state.

x	Model	P	W	Tr
	Pletchov & Gerya 1998			
	Ariskin et al. 1993			
	Langmuir et al. 1992			
	Ariskin Barmina 1990	c	c	
	Weaver & Langmuir 1990			
	Nielsen 1985			
	Nielsen & Dungan 1983			
	Drake 1976			

Figure 4.8. Window for choosing a model for plagioclase-melt equilibrium with 'c' in columns 'P' and 'W' next to the chosen model indicating that a pressure correction and an H₂O correction were set.

Phase	Model	P	W	Tr
Olivine	Herzberg & O'Hara 2002	Y		Y
Plagioclase	Ariskin Barmina 1990	c	c	
Clinopyroxene	Langmuir et al. 1992	Yc	c	
Orthopyroxene	Bolikhovskaya et al. 1996	Y		
Pigeonite	Bolikhovskaya et al. 1996	Y		
Spinel	Press to Select			
Ilmenite	Press to Select			
Magnetite	Press to Select			
Sulfide	O'Neill 2021			Y
Fluid	Iacono-Marziano et al 2012	Y		Y

☒ Force Pl-Ol cotectic

Figure 4.9. The 'Models for phase-melt equilibrium' subsection of the Parameters Section showing selected mineral-melt models; whether the selected models incorporate pressure, H₂O and trace elements ('Y'); and which models have corrections set for the effects of pressure and H₂O ('c').

The 'Mineral-melt models' subsection of the Parameters Section (Fig. 1.1) displays the models chosen for each mineral and uses columns 'P', 'W', and 'Tr' to indicate whether the chosen models incorporate effects of pressure and/or H₂O, and/or trace elements, and whether any user-defined correction are set for the effects of pressure and melt H₂O contents. Capital 'Y' is used to indicate that a model includes a corresponding effect, whereas 'c' is used to indicate that a correction is set (Fig. 4.9).

4.1.1.5. Calculating an olivine - plagioclase ± clinopyroxene cotectic crystallisation.

Petrolog4 offers an option of forcing the starting composition on an olivine-plagioclase (+/- clinopyroxene) cotectic by adjusting melt H₂O content, following the method of Danyushevsky (2001). The essence of the approach is to first calculate the amount of H₂O which is required for the starting composition to lie on an olivine-plagioclase cotectic, and then to model crystallisation with this H₂O content in the starting composition, so that the composition is cotectic from the onset of crystallisation. (see Danyushevsky, 2001 for a detailed description of the approach). The set of minerals is limited to olivine, plagioclase and clinopyroxene, and the set of models is limited to those from Danyushevsky (2001).

To use this option, check the 'Force Pl-Ol cotectic' checkbox in the 'Models for phase-melt equilibrium' subsection of the Parameters Section (Fig. 4.9).

Note: This option should be used for MORB and BABB compositions only, as the models of Danyushevsky (2001) have not been calibrated outside that compositional range.

Note: When using this option, calculation pressure should be set at a value that ensures that the melt H₂O content required for modelling along a cotectic is less than the saturation value (see section 4.1.4).

4.1.2. Setting extent of fractionation for each phase

Petrolog4 allows for a specific extent of fractionation to be set for each phase using the 'Extent of fractionation (%)' subsection of the Parameters Section (Figs. 1.1, 1.2, 2.2). By default, a value of 100% is assigned to each phase, corresponding to the case of pure fractional crystallisation. When modelling pure fractional crystallisation, a phase is 'removed' from contact with melt and placed into the 'cumulate' part of the system, thus retaining its original composition.

If 0% is assigned to a phase, this corresponds to pure equilibrium crystallisation. When modelling equilibrium crystallisation, the total amount of the crystallised phase remains in equilibrium with the residual melt, thus continuously changing its composition. No 'cumulate' is formed during equilibrium crystallisation.

When a number between 0 and 100 is entered for a phase, this proportion of the phase is continuously 'removed' from contact with the melt preserving its composition, whereas the remainder of the phase re-equilibrates with the continuously evolving melt. See Danyushevsky and Plechov (2011) for further details of the approach.

4.1.3. Setting pressure

Pressure to be used during calculations is set in the 'Pressure' subsection of the Parameters Section (Figs. 1.1, 1.2, 2.2). A value at the onset of calculations (in kbar) can be set in the 'Initial P (kbar)' textbox within this subsection.

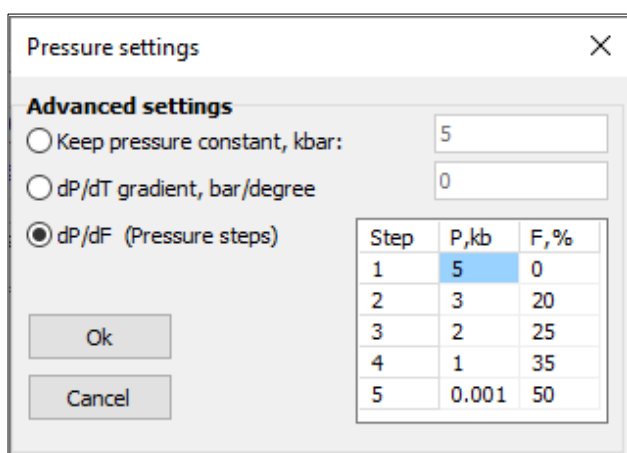


Figure 4.10. The 'Pressure settings' window showing three available options for controlling pressure during calculations.

Note: The data file can contain a column that defines pressure values to be used in calculations that can differ for each analysis. The values should be in kbar (1 kbar = 0.1 GPa). This column should have the following name in the header row: P_KBAR or P_KBAR or PRESSURE.

To define changes to crystallisation pressure during calculations, click on the blue text label below the 'Set Pressure behaviour:' text label in this subsection. This will open the 'Pressure settings' pop-up window (Fig. 4.10).

By default, the 'Keep pressure constant' option is chosen.

The 'dP/dT gradient, bar/degree' option allows for pressure to be continuously changed at a fixed rate as a function of temperature. A positive value corresponds to decreasing pressure during crystallisation. If pressure reaches 1 bar before the end of the calculations, it will

remain at 1 bar for the remainder of the calculations. Setting a negative value for the gradient would result in pressure increasing during crystallisation calculations.

The 'Pressure steps' option allows for changing pressure during calculations as a function of the extent of crystallisation. Up to four steps with specific dP/dF values can be set. The dP/dF value for an interval is calculated from the P and F values set as the boundary conditions for the interval. The dP/dF value can equal 0 (pressure is constant) for any number of steps. To set it to 0, the 'P, kb' value should be the same at the start and end of a crystallisation step. If the F value at the end of the last step is lower than the final F value during calculations, the pressure value at the last step will be used until the end of crystallisation calculations.

The displayed text in the blue text label in the subsection reflects the chosen pressure option: 'Keep constant', 'dP/dT = 'Value'', or 'dP/dF'.

4.1.4. Setting fluid, sulphur, zircon and apatite saturation models

Performing calculations in Petrolog4 requires that models for melt saturation in fluid, sulphur, apatite and zircon are defined. When software starts, default saturation models are automatically assigned. The assigned

models are displayed in the 'Saturation Models' subsection of the Parameters section of the Main form (Figs 1.1, 1.2, 2.2). The selected models can be changed by clicking the blue 'Change Saturation Models:' text label in this subsection, to open the 'Melt Saturation Models' pop-up window (Fig. 4.11). The available models are listed in Appendix 1.

Click 'Ok' to save the chosen models. Pressing 'Cancel' closes the form without applying any changes.

When the concentrations of volatile elements (H_2O and CO_2), reduced sulphur (S^{2-}), oxidised sulphur (S^{6+}), phosphorus (P) or zirconium (Zr) in the melt exceed their solubility values according to the chosen model, this leads to appearance of a separate fluid, immiscible sulphide melt, sulphate, apatite or zircon phase, respectively. Similarly to silicate minerals, the fluid, sulphide, sulphate, apatite and zircon phases may either remain in the magma or fractionate (see section 4.1.2).

Petrolog4 also offers an option to perform calculation under forced fluid-saturated and sulphide-saturated conditions. To use these options, check the 'Fluid saturated' and 'Sulphide saturated' checkboxes within the 'Starting melt composition' subsection of the Parameters section of the Main form (Figs. 1.1, 1.2, 2.2). If neither H_2O nor CO_2 are present in the starting composition when the 'Fluid saturated' option is used, a pure- H_2O system will be assumed, unless 'pure CO_2 ' fluid model is selected, in which case a pure CO_2 system will be assumed.

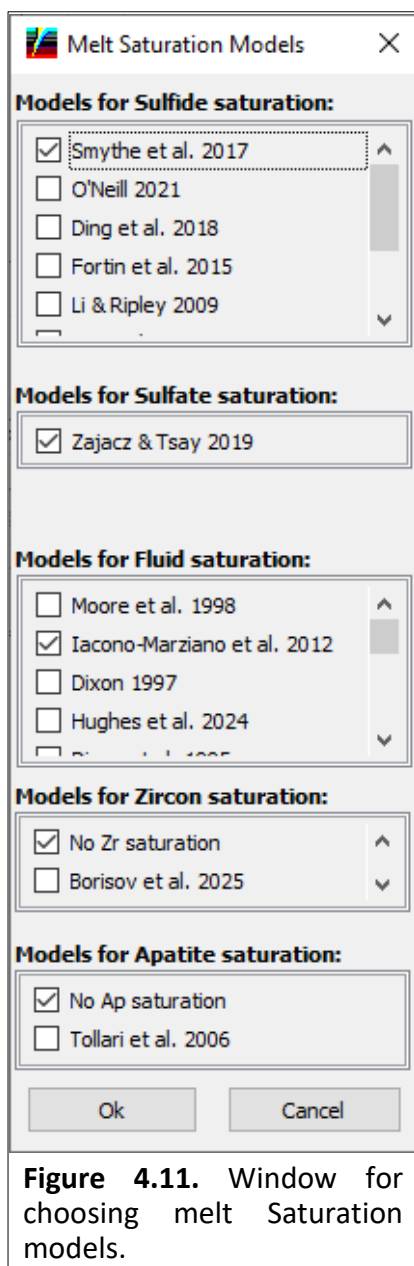
Note: When H_2O and/or CO_2 are present in the starting composition, the user must select a fluid-melt equilibrium model to enable calculations, even if it is not expected that fluid saturation will be reached. When the starting melt composition is fluid oversaturated at the pressure chosen for calculation, melt H_2O and CO_2 contents will be adjusted to reflect fluid saturation at the chosen pressure.

Note: If during calculations the CO_2 content of the silicate melt becomes less than 0.1 ppm, the calculations will stop as the fluid-melt equilibrium models available in the current version cannot handle such compositions.

Note: When 'Iacono-Marziano et al 2012' model for fluid composition is selected, the fluid saturation model 'Iacono-Marziano et al 2012' will be automatically selected (and vice versa).

Note: When 'Holloway & Blank 1994' or 'Dixon 1997' or 'Allison et al. 2019' models for fluid composition are selected, the fluid saturation models 'Holloway & Blank 1994' or 'Dixon 1997' or 'Allison et al. 2019', respectively, will be automatically selected (and vice versa). If the melt CO_2 content decreases below 10 wt. ppm, calculations will be stopped as these models were not meant to be used with such compositions.

Note: When the 'Pure H_2O ' model for fluid composition is selected, the fluid saturation model 'Moore et al. 1998' will be automatically selected, unless a different model for the pure- H_2O system is already selected. When either 'Holloway and Blank 1994 (H_2O)' or 'Moore et al. 1998' or Shishkina et al. 2014 (H_2O)' or Lesne et al. 2014 (H_2O)' models are selected, the 'Pure H_2O ' model for fluid composition will be automatically selected.



Note: When the 'Pure CO₂' model for fluid composition is selected, the fluid saturation model 'Shishkina et al. 2014 (CO₂)' will be automatically selected. When 'Shishkina et al. 2014 CO₂' model is selected, the 'Pure CO₂' model for fluid composition will be automatically selected.

Note: When S is present in the starting composition, the user must select a sulphide-melt and a sulphate-melt equilibrium models to enable calculations, even if it is not expected that sulphide or sulphate saturation will be reached. When the starting composition is S-oversaturated, the S content will be adjusted to match saturation.

Note: By default, Petrolog4 starts with 'No Ap saturation' and 'No Zr saturation' models chosen. Thus, P- and/or Zr-oversaturation would not be checked during calculations, unless the user explicitly selects an apatite (and / or zircon) saturation model, or an apatite- (zircon-) melt equilibrium model.

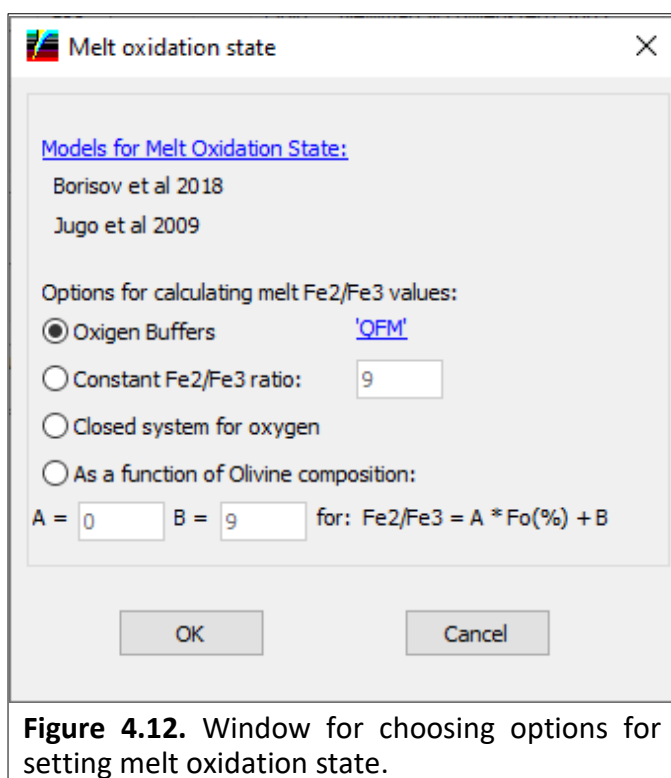


Figure 4.12. Window for choosing options for setting melt oxidation state.

4.1.5. Setting melt oxidation state

The melt oxidation state (i.e., the proportions of Fe²⁺ / Fe³⁺ and S²⁻ / S⁶⁺ in the melt) during calculations is set in the 'Oxidation state' subsection of the Parameters Section (Figs. 1.1, 1.2, 2.2). The currently chosen method for controlling melt oxidation state is displayed in the blue text label below 'Calculations performed using:' text label. When Petrolog4 starts, the quartz-magnetite-fayalite (QFM) oxygen buffer is selected by default. To change the selected method, click on the blue text label with the currently selected method, to open the 'Melt oxidation state' pop-up window (Fig. 4.12).

Four options for controlling melt oxidation state are available: I) calculation assuming a closed system for oxygen; II) calculation along an oxygen buffer; III) calculation with a constant Fe²⁺/Fe³⁺ value; and IV) defining melt oxidation state as a function of liquidus olivine composition (Fig. 4.12).

Performing calculations in Petrolog4 requires that models for Fe and S oxidation states in the silicate melt are defined. When software starts, default models are automatically selected. The selected models are displayed in the bottom part of the 'Oxidation state' subsection of the Parameters section of the Main form (Figs 1.1, 1.2, 2.2). The selected models can be changed by clicking the blue 'Change Oxidation Models:' text label in this subsection to open the 'Melt Oxidation State Models' pop-up window (Fig. 4.13). The available models are listed in Appendix 1. This form can also be opened from the 'Melt Oxidation State' window (Fig. 4.12).

I. When calculations are performed assuming a closed system for oxygen, the melt oxidation state is controlled by 1) removal of ferrous and ferric Fe by crystallising silicate and oxide minerals; 2) removal of ferrous Fe and S²⁻ by separation of an immiscible sulphide in sulphide-saturated magmas; and 3) by degassing of sulphur species in fluid-saturated magmas. Petrolog4 maintains equilibrium between oxidation states of Fe and S. Petrolog4 does not consider the presence of Fe⁰ when calculations are performed at strongly reduced conditions.

Note: Sulphur oxidation state in the starting composition is calculated from the melt oxidation state as defined either by the oxygen fugacity or the oxidation state of Fe, regardless of S speciation defined in the starting composition (i.e., regardless of whether sulphur content is entered as S or SO₃).

Note: Choosing the 'Closed system for oxygen' option requires that ferric and ferrous Fe contents are defined in the starting composition. If the ferrous Fe content in the starting composition is 0, the calculations will be performed following the Magnetite-Hematite buffer of oxygen fugacity. If the ferric Fe content is set to 0, the calculations will be performed assuming that all Fe and all S in the starting composition

are in the reduced form and no oxidised species will be present during fractionation. This latter is identical to choosing Fe₃=0 'buffer' option (Fig. 4.14).

II. When calculations are performed along an oxygen buffer, to change the selected buffer click on the blue text label next to the 'Oxygen Buffers' bullet point that shows the currently selected buffer (Fig. 4.12). This opens the 'Oxygen Buffers' pop-up window (Fig. 4.14). This window contains a plot comparing oxygen fugacity values along various buffers. Buffer equations are listed in Appendix 1.

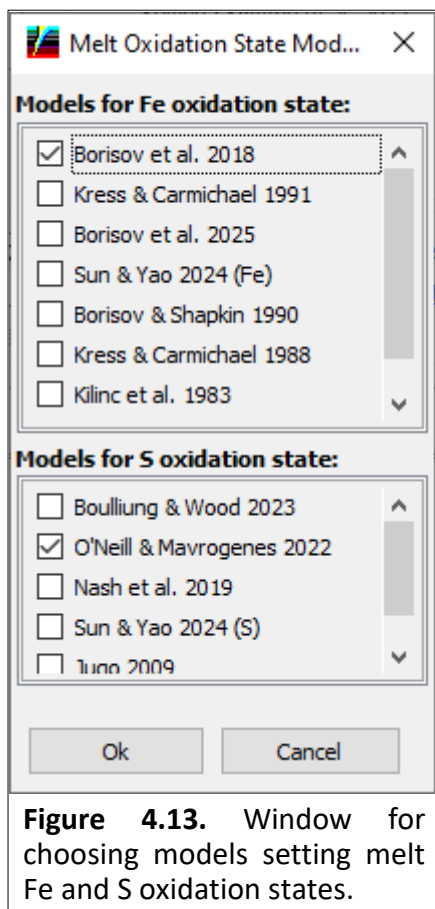


Figure 4.13. Window for choosing models setting melt Fe and S oxidation states.

To choose a buffer click on one of the check boxes next to the buffer name. You can also specify a shift from the buffer in log₁₀ units of fO₂ by specifying a positive or negative value in the 'Buffer shift (log units):' text

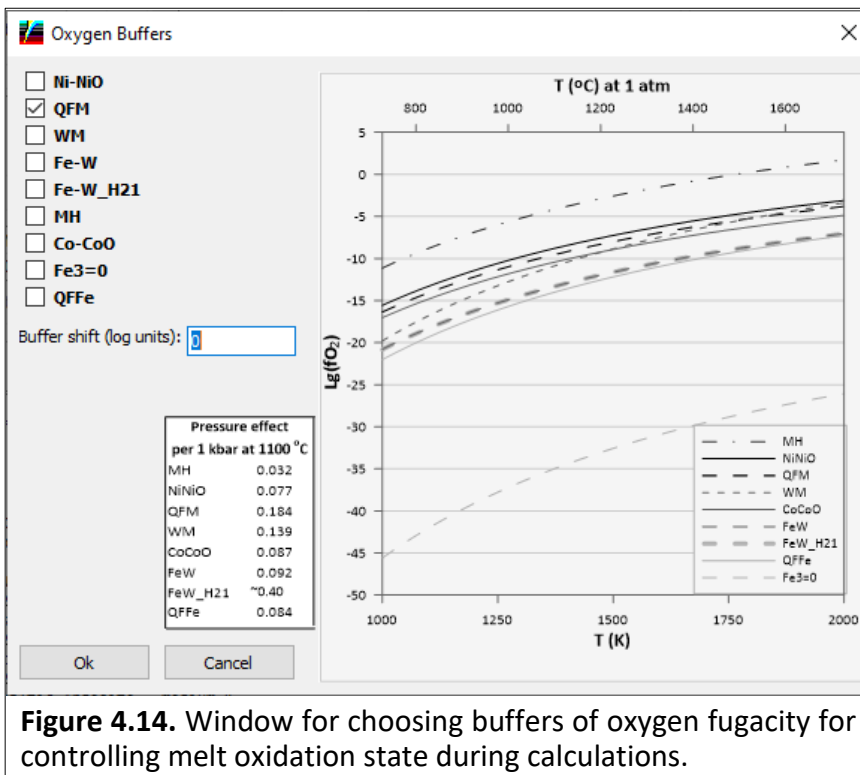


Figure 4.14. Window for choosing buffers of oxygen fugacity for controlling melt oxidation state during calculations.

box. The equations for each of the buffers is listed in Appendix 1.

Close this window by pressing the 'OK' button. Pressing the 'Cancel' button closes the window without applying the changes made.

When using an oxygen buffer to define melt oxidation state, the Fe²⁺ / Fe³⁺ and S²⁻ / S⁶⁺ values in the melt will be calculated from the oxygen fugacity value corresponding to the chosen buffer, following the chosen models for the oxidation state.

III. When using a constant Fe²⁺ / Fe³⁺ value to set melt oxidation state, oxygen fugacity and S²⁻ / S⁶⁺ are calculated from the Fe²⁺ / Fe³⁺ value of the melt following the chosen models for Fe and S oxidation states (Fig. 4.13).

IV. If the melt oxidation state is defined as a function of liquidus olivine composition (Fig. 4.12), specify values for coefficients A and B for the equation (Fe²⁺/Fe³⁺)_{melt} = A*Fo + B, where Fo is the proportion of forsterite in the liquidus olivine in mol%. For a detailed description of this technique, see Danyushevsky and Sobolev, 1996. When using this option to set melt oxidation state, oxygen fugacity and S²⁻ / S⁶⁺ are calculated from the Fe²⁺ / Fe³⁺ value of the melt following the chosen model for Fe oxidation state (Fig. 4.13).

Note: This option is only available when olivine has been chosen for calculations in the 'Models for phase-melt equilibrium' subsection window.

4.1.6. Choosing models to calculate melt physical properties

Petrolog4 calculates melt density and viscosity during melt evolution. To choose from the available models, click on the blue text labels within the 'Melt physical properties' subsection of the Parameters Section (Figs.

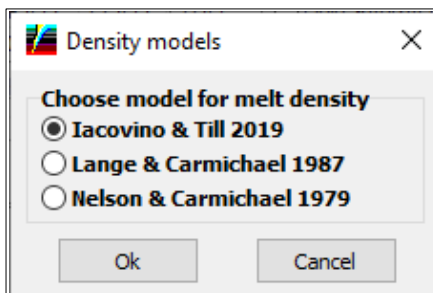


Figure 4.15. Window for choosing melt density models.

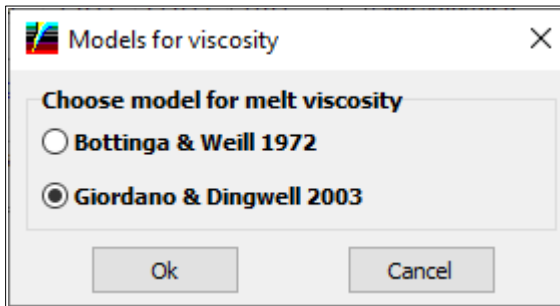


Figure 4.16. Window for choosing melt viscosity models.

1.1, 1.2, 2.2). Clicking on the blue text label next to 'Density:' opens the 'Density Models' pop-up window (Fig. 4.15). Choose the desired model by pressing on one of the radio buttons next to model names. The available models are listed in Appendix 1. Close the

window by pressing the 'Ok' button. Pressing the 'Cancel' button closes the window without applying the changes made.

Clicking on the blue text label next to 'Viscosity:' opens the 'Models for Viscosity' pop-up window (Fig. 4.16). Choose the desired model by pressing on one of the radio buttons next to model names. The available models are listed in Appendix 1. Close the window by pressing the 'Ok' button. Pressing the 'Cancel' button closes the window without applying the changes made.

4.1.7. Setting calculation step

A value for the calculation step is set in the 'Calculation step' text box inside the 'Calculation Parameters' sub-section in the Parameters Section (Figs. 1.1, 1.2, 2.2). The calculation step determines the amount (in wt.%) by which the melt mass decreases at each step of crystallisation calculations. The smaller the calculation step is the more precise the calculations are, but this also leads to the calculations taking longer. The default value of 0.01% of the amount of melt on each step provides acceptable precision and reasonably short calculation times. For implications of using larger or smaller crystallisation steps see Danyushevsky and Plechov, 2011. It is not recommended to increase the calculation step.

Note: The algorithm used in Petrolog4 is designed with an assumption that the output of the intermediate states of the system during calculations would occur at frequencies which are at least 2 orders of magnitude larger than the calculation step. For example, if the calculation step is set to 0.01%, the smallest recommended output frequency is 1% of the extent of crystallisation.

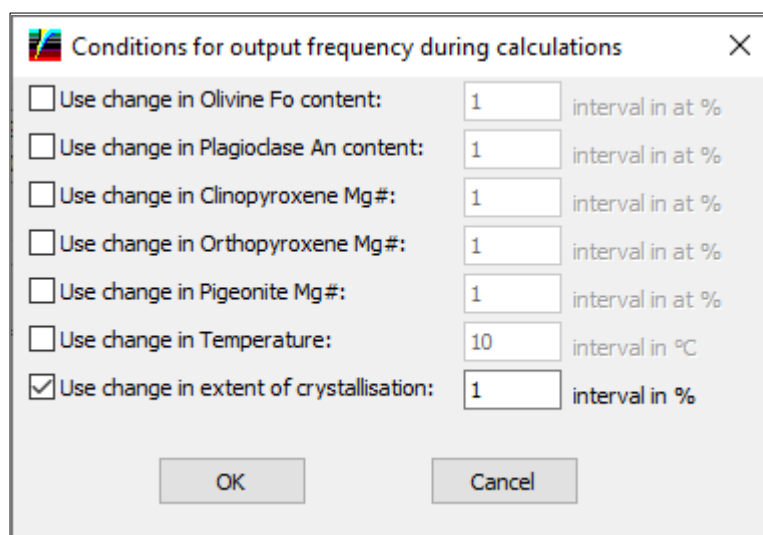


Figure 4.17. The 'Conditions for output frequency during calculations' window showing options available for setting conditions for the output of the intermediate states of the system during calculations.

4.1.8. Setting conditions for the frequency of results output during calculations

Petrolog4 offers several options for setting output frequency of the intermediate states of the system during calculations. The default setting is 1 wt.% of crystallisation. To change this setting, click on the blue text label below 'Define output frequency:' text label inside the 'Calculation Parameters' sub-section in the Parameters Section (Figs. 1.1, 1.2, 2.2). This will open the 'Conditions for output frequency during calculations' pop-up window (Fig. 4.17). Several options can be set simultaneously, and the program will report the intermediate states of the system satisfying all the selected criteria. The results are displayed in the Output Section of the Main Form (Fig. 1.2, see Section 4.1.9) and saved in several files (see Section 4.3).

Close the window by pressing the 'Ok' button. Pressing the 'Cancel' button closes the window without applying the changes made. The blue label will display the chosen option(s).

4.1.9. Output of results on screen during calculations

When calculations start, a summary of all calculations parameters is displayed (Table 4.1). If any volatile or trace elements are included in the starting composition, the summary includes a table with all distribution coefficients (Ds) that will be used during calculation.

Note: If any of the volatile elements included in calculations are the major elements in some of the included phases (e.g., O in silicates and H₂O-CO₂ fluids, H and C in H₂O-CO₂ fluids, and reduced S in immiscible sulphide melts) their concentrations in the relevant phases will be determined using the chosen models of phase-melt equilibrium, and thus D values are not applicable to these elements in such phases (n/a) is listed in the table with Ds (see Table 4.1).

The summary of parameters is followed by the starting composition ('Start'; Table 4.2). If sulphur is present in the starting composition, the composition is checked for sulphide-oversaturation following the chosen model for sulphide saturation before calculations begin. If oversaturation is observed, the S concentration in the starting composition is adjusted to match sulphide saturation following the starting oxidation state. Similarly, if H₂O and / or CO₂ are present in the starting composition, the composition is checked for fluid-oversaturation following the chosen model for fluid saturation before calculations begin. If oversaturation is observed, the H₂O and / or CO₂ concentrations in the starting composition are adjusted to match fluid saturation at the starting pressure. A message stating the above is displayed above the starting composition (Table 4.2).

If the calculations are performed at the conditions of sulphide and /or fluid saturation, the concentrations of S, H₂O and CO₂ are changed to reflect saturation following the chosen models for sulphide and /or fluid saturation. Messages stating the above are displayed above the starting composition (Table 4.2.). In the example shown in Table 4.2, the concentration of sulphur in the starting composition was above saturation at the chosen calculation parameters, and thus it has been reduced, whereas the concentrations of H₂O and CO₂ were below saturation at the chosen parameters, and thus they were increased.

The composition that will be used as the starting composition ('Melt', see Table 4.2) is listed below the 'Start' composition. The default Petrolog4 output for chemical composition is using components for major and volatile elements (e.g., oxides for silicate and oxide minerals and H₂O-CO₂ fluid, and mono-sulphides for an immiscible sulphide melt, see the upper section of Table 4.2). Reduced S is taken to be coupled to ferrous Fe in the melt phase, and thus its concentration in the melt is represented by the FeS component. Trace elements are displayed using elemental concentrations and the total amount of oxygen allocated to the trace elements is shown in the O_wt% column.

The user can choose to display results of calculations in elemental concentrations for all chemical elements (see lower section of Table 4.2). In this case, the O_wt% column would display the total O concentration and the Fe2 column will display the total ferrous Fe concentration. To switch between component and elemental outputs, use the 'Use Components for Screen Output' option (see Section 1.2).

Table 4.3 presents the state of the system after 2 % of crystallisation, i.e, when the mass of the melt is 98% of the starting mass, with other phases comprising 2 % of the initial mass of the starting melt. The first line of the output is the magma composition at the given stage of evolution. The magma composition represents the combined composition of the melt and all phases residing with the melt, i.e, the phases that are not fractionating from the melt. In the example used here, 20% of crystallising olivine would remain in the magma, 30 % of pyroxenes and 50% of plagioclase, fluid and immiscible sulphide melt (see Table 4.1).

The second line is the composition of the melt. When some proportions of the crystallising phases remain in the magma (as is the case for this example), the composition of the magma is different from the composition of the melt.

Below the melt are the compositions of all phases that are currently crystallising from the melt. In the example shown in Table 4.3, only olivine, fluid and sulphide phase have formed from the melt after 2% of crystallisation.

When components are used for the outputs, the compositions of fluid and sulphide melt are shown separately from other phases as the components in these two phases are different (see the upper section of Table 4.3). In the immiscible sulphide melt all major and trace elements are coupled with reduced sulphur. If oxygen is present, it is coupled with ferrous Fe forming the FeO component. Column 'S_ppm' displays the amount of sulphur coupled to trace elements. If H, C and oxidised sulphur are present in sulphide phase, they are coupled with oxygen.

In the fluid phase, reduced sulphur is coupled with hydrogen forming the H₂S component, and oxidised sulphur is +4 rather than +6, thus forming the SO₂ component. When the results of calculations are displayed in elemental concentrations (see the lower section of Table 4.3), the value for each element in each phase displays the total elemental concentration in this phase.

Note: When output using components is chosen, the magma composition in Table 4.3 is shown using the elemental concentrations. This is because when fluid containing S and / or immiscible sulphide melt are present in the magma, it is impossible to display the combined composition of all phases in the magma using components. When neither fluid containing S nor sulphide are present in the magma, its composition is shown using components.

The phase compositions are followed by a line with phase compositional parameters of the crystallising phases (mol% forsterite (Fo) for Olivine; mol% anorthite (An) for Plagioclase; Mg# ($100 \cdot \text{Mg}/(\text{Mg}+\text{Fe})$) for Clinopyroxene; Orthopyroxene; Pigeonite; Ilmenite and Magnetite; Cr# ($100 \cdot \text{Cr}/(\text{Cr}+\text{Al})$) for Spinel; Fe# ($100 \cdot \text{Fe}/(\text{Ni}+\text{Fe})$) for sulphide; CO₂# ($100 \cdot \text{CO}_2/(\text{CO}_2+\text{H}_2\text{O})$ in mol units) for fluid; Ca# ($100 \cdot \text{Ca}/(\text{Ca}+\text{Ba})$) for sulphate; Si# ($100 \cdot \text{Si}/(\text{Si}+\text{Al})$) for quartz; K# ($100 \cdot \text{K}/(\text{K}+\text{Na})$) for orthoclase and leucite; Na# ($100 \cdot \text{Na}/(\text{K}+\text{Na})$) for nepheline; Hf# ($100 \cdot \text{Hf}/(\text{Hf}+\text{Zr})$) for zircon; Ca# ($100 \cdot \text{Ca}/(\text{Ca}+\text{Sr}+\text{Ba}+\text{REE})$) for apatite.

The next line displays melt temperature, oxygen fugacity (as both an absolute value and a shift from the chosen reference buffer (Fig. 1.3)), and pseudo-liquidus temperatures for all minerals involved in calculations.

The next line contains weight proportions of all phases in the magma.

The next line shows crystallisation pressure, melt density and viscosity.

When some proportions of some of the phases fractionate from the magma (as is the case for the example in Tables 4.1, 4.2, 4.3), the compositions of fractionated phases are shown under the line with crystallisation pressure. The first line repeats component or element names. Below it, the composition of the combined fractionated phases called 'Cumulate' is displayed.

Note: When fluid and / or immiscible sulphide melt are present among fractionated phases, the bulk composition of the 'Cumulate' is shown using elemental concentrations even if the output using component concentrations is chosen. This is because in such a case it is impossible to display the combined composition of fractionated phases (the 'Cumulate' composition) using components. When neither fluid nor sulphide are present, the composition of the 'Cumulate' is shown using components when the output using component concentrations is chosen.

Lines below the 'Cumulate' composition show bulk compositions of all fractionated phases at the given extent of melt evolution. The bulk compositions for each phase are calculated by mass-balancing fractionated compositions continuously formed during crystallisation.

Note: To include the bulk composition of each phase in the cumulate in the output of results into files, use option 'Add export of cumulus phases to files' (see Section 1.2).

The next line below the bulk composition of each phase shows bulk fractionated phase compositional parameters. In most cases these will be higher (i.e., skewed towards the compositions of earlier formed crystals) than the compositions currently crystallising from the melt (see Danyushevsky and Plechov, 2011 for more details).

The last line of the output contains weight proportions of all phases in the cumulate.

Table 4.4 presents the state of the system after 40 % of crystallisation. At this extent of crystallisation, plagioclase and clinopyroxene joined the crystallising assemblage. Since plagioclase, fluid and sulphide are all set to fractionate at 50%, their amount in the magma and cumulate are equal, whereas there are larger amounts of olivine and clinopyroxene in the fractionated phases than in the magma since they were set to fractionate at 80% and 70%, respectively.

Table 4.1. Example output: Calculation parameters at the start of calculation

Modelling Crystallisation

Phases chosen for calculations are:

Olv, Plg, Cpx, Opx, Pig, Slf, Fld, Sft

The model used for Olv is: Herzberg & O'Hara 2002

Olv fractionation is: 80.00 %

The correction for the effect of H2O on Olv liquidus temperature is calculated using Petrolog default settings

The model used for Plg is: Ariskin et al. 1993

Fe content in plagioclase is calculated after Lundgaard & Tegner (2004)

Plg fractionation is: 50.00 %

The correction for the effect of H2O on Plg liquidus temperature is calculated using Petrolog default settings

The model used for Cpx is: Ariskin et al. 1993

Cpx fractionation is: 70.00 %

The correction for the effect of H2O on Cpx liquidus temperature is calculated using Petrolog default settings

The model used for Opx is: Bolikhovskaya et al. 1996

Opx fractionation is: 70.00 %

The correction for the effect of H2O on Opx liquidus temperature is calculated using Petrolog default settings

The model used for Pig is: Bolikhovskaya et al. 1996

Pig fractionation is: 70.00 %

The correction for the effect of H2O on Pig liquidus temperature is calculated using Petrolog default settings

The model used for Slf is: Kiseeva & Wood 2015

Slf fractionation is: 50.00 %

The correction for the effect of H2O on Slf liquidus temperature is calculated using Petrolog default settings

The model used for Fld is: Iacono-Marziano et al 2012

Fld fractionation is: 50.00 %

The model used for Sft is: Ca sulphate

Sft fractionation is: 50.00 %

The correction for the effect of H2O on Sft liquidus temperature is calculated using Petrolog default settings

Fe2O3 in the melt is calculated using an assumption of closed system for oxygen

f(O2) is calculated following the model of Borisov et al 2018

Sulfur speciation in the melt is calculated using the model of O'Neill & Mavrogenes 2022

Calculations are performed assuming fluid saturation

Fluid saturation of the melt is calculated using the model of Iacono-Marziano et al 2012

Calculations are performed assuming sulfide saturation

Sulfide saturation of the melt is calculated using the model of O'Neill 2021

Sulfate saturation of the melt is calculated using the model of Zajacz & Tsay 2019

Initial Pressure = 5 kbar

During calculations Pressure is changed at 20 % crystallisation to 3 kbars

at 25 % crystallisation to 2 kbars

at 35 % crystallisation to 1 kbars

at 50 % crystallisation to 0 kbars

Melt density is calculated following the model of Lange & Carmichael 1987

Melt viscosity is calculated following the model of Giordano & Dingwell 2003

Parameters to stop calculations at:

Final degree of fractionation: 70 %

The amount of a mineral phase which will be extracted from

100% of melt on each step is: 0.01 %

Ds for phases:

Mineral	H	C+	S-	S+	O	Co	Ni	Cu	Rb	Sr	Ba	Yb
Olv	0	0	0	0	n/a	Beatt91	Herzb02	0	0.001	0.01	0	0
Plg	0	0	0	0	n/a	0	0	0	0.1	Bl_Wo91	Bl_Wo91	0
Cpx	0	0	0	0	n/a	0.2	1	0	0.05	0.07	0.03	Wo_Bl97
Opx	0	0	0	0	n/a	0.8	1.5	0	0.02	0.05	0.015	0
Pig	0	0	0	0	n/a	0.8	1.2	0	0.03	0.05	0.02	0
Slf	0	0	n/a	0	KiWd2015	KiWd2015	KiWd2015	KiWd2015	0	0	0	0
Fld	n/a	n/a	Ding2023	Ding2023	n/a	0	0	0	0.2	0.1	0.3	0
Sft	0	0	0	n/a	n/a	0	0	0	0	0	1.5	0

Table 4.2. Example output: The starting composition

Output using component concentrations

The starting composition "Analysis2" has been adjusted for the chosen oxidation state, checked for fluid and sulfide saturation, and recalculated to 100 wt%

Since "Fluid saturated" option is selected, H₂O and/or CO₂ contents in the starting composition have been adjusted to match fluid saturation.

Since "Sulfide saturated" option is selected, S content in the starting composition has been adjusted to match sulfide saturation.

	SiO ₂	TiO ₂	Al ₂ O ₃	Fe ₂ O ₃	FeO	MnO	MgO	CaO	Na ₂ O	K ₂ O	P ₂ O ₅	Cr ₂ O ₃	FeS*_ppm	H ₂ O_wt%	CO ₂ _ppm	S_ppm	SO ₃ _ppm	O_wt%	Co_ppm	Ni_ppm	Cu_ppm	Rb_ppm	Sr_ppm	Ba_ppm	Yb_ppm
Start	51.00	1.30	16.00	1.00	7.78	0.18	11.00	10.00	1.70	0.70	0.11	0.11	2742.0	0.500	3000.0		0.0	0.011	55.0	200.0	150.0	9.0	86.0	3.0	10.0
Melt	49.96	1.27	15.67	0.98	7.65	0.18	10.78	9.80	1.67	0.69	0.11	0.11	2289.6	0.515	3414.7		2.2	0.010	53.9	195.9	146.9	8.8	84.2	2.9	9.8

Output using elemental components

The starting composition "Analysis2" has been adjusted for the chosen oxidation state, checked for fluid and sulfide saturation, and recalculated to 100 wt%

Since "Fluid saturated" option is selected, H₂O and/or CO₂ contents in the starting composition have been adjusted to match fluid saturation.

Since "Sulfide saturated" option is selected, S content in the starting composition has been adjusted to match sulfide saturation.

	Si	Ti	Al	Fe ₃	Fe ₂	Mn	Mg	Ca	Na	K	P	Cr	H_ppm	C+_ppm	S-_ppm	S+_ppm	O_wt%	Co_ppm	Ni_ppm	Cu_ppm	Rb_ppm	Sr_ppm	Ba_ppm	Yb_ppm
Start	23.84	0.78	8.47	0.70	6.22	0.14	6.63	7.15	1.26	0.58	0.05	0.08	555.6	818.7	1000.0	0.0	45.832	55.0	200.0	150.0	9.0	86.0	3.0	10.0
Melt	23.36	0.76	8.30	0.69	6.09	0.14	6.50	7.00	1.24	0.57	0.05	0.07	571.7	931.8	835.0	0.9	44.963	53.9	195.9	146.9	8.8	84.2	2.9	9.8

Note: When components are used for output and the starting composition does not contain any trace or volatile elements except O, the O_wt% column is not displayed.

Note: When components are used for output and the starting composition does not contain any trace elements but contains volatile elements in addition to O, the O_wt% column displays a 0 value.

Note: When components are used for output and the starting composition does not contain sulphur, the FeS*_ppm, S_ppm and SO₃_ppm columns are not displayed

Note: '*' in the name of the FeS*_ppm column indicates that if reduced sulphur is present at a trace level in plagioclase or nepheline, it is coupled to Na and this column would display the concentration of Na₂S in ppm; if reduced sulphur is present at a trace level in orthoclase or leucite, it is coupled to K and this column would display the concentration of K₂S in ppm; if reduced sulphur is present at a trace level in quartz, it is coupled to Si and this column would display the concentration of SiS₂ in ppm; if reduced sulphur is present at a trace level in sulphate, it is coupled to Ca and this column would display the concentration of CaS in ppm.

Table 4.3. Example output: An intermediate state of the system during calculations at 2% of crystallisation of the starting composition (Tables 4.1, 4.2)

Output using component concentrations

	Si	Ti	Al	Fe3	Fe2	Mn	Mg	Ca	Na	K	P	Cr	H_ppm	C+_ppm	S-_ppm	S+_ppm	O_wt%	Co_ppm	Ni_ppm	Cu_ppm	Rb_ppm	Sr_ppm	Ba_ppm	Yb_ppm		
Magma	23.43	0.78	8.43	0.70	6.05	0.14	6.15	7.11	1.26	0.58	0.05	0.07	580.9	899.5	837.8	1.3	44.989	52.0	162.2	145.0	9.0	85.6	3.0	10.0		
	SiO2	TiO2	Al2O3	Fe2O3	FeO	MnO	MgO	CaO	Na2O	K2O	P2O5	Cr2O3	FeS*_ppm	H2O_wt%	CO2_ppm	S_ppm	S03_ppm	O_wt%	Co_ppm	Ni_ppm	Cu_ppm	Rb_ppm	Sr_ppm	Ba_ppm	Yb_ppm	
Melt	50.17	1.30	15.99	1.00	7.58	0.18	10.05	9.99	1.70	0.70	0.11	0.11	2279.0	0.525	3135.6		2.9	0.009	51.5	150.1	141.0	9.0	85.9	3.0	10.0	
Olv	40.33	0.04	0.11	0.00	11.46	0.20	47.28	0.29	0.00	0.00		0.04						0.052	168.4	1746.0		0.0	0.9			
	SiO2	TiO2	Al2O3	Fe2O3	FeO	MnO	MgO	CaO	Na2O	K2O	P2O5	Cr2O3		H2O_wt%	CO2_ppm	H2S_ppm	S02_ppm	O_wt%	Co_ppm	Ni_ppm	Cu_ppm	Rb_ppm	Sr_ppm	Ba_ppm	Yb_ppm	
Fld														0.384	994615.0	106.6	1421.1	0.000				1.8	8.6	0.9		
	SiS2	TiS2	Al2S3	Fe2S3	FeS	MnS	MgS	CaS	Na2S	K2S	P2S5	Cr2S3	FeO_ppm	H2O_wt%	CO2_ppm	S_ppm	S03_ppm	O_wt%	Co_ppm	Ni_ppm	Cu_ppm	Rb_ppm	Sr_ppm	Ba_ppm	Yb_ppm	
Slf					49.57								45037.9			135406.4		2612.2	180124.9	141095.4						
Fo= 88.025 Kd(Olv-Melt)= 0.314; Fe#Slf= 67.122; CO2#Fl= 99.064; T=1213.3 (Olv); Lg(fO2)=-8.52 dQFM=-0.73; TPlg=1115.8 TCpx=1154.9 T0px=1191.4 TPig=1167.7 TMgt=975.4 Amounts (wt%) of phases in magma: Melt 97.9991; Olv 0.3920; Slf 0.0032; Fld 0.01718; Pressure: 4.800 kbar; Density: 2.677 g/cm3; Viscosity: v=26 poise; ln(v)=3.2																										
	Si	Ti	Al	Fe3	Fe2	Mn	Mg	Ca	Na	K	P	Cr	H_ppm	C+_ppm	S-_ppm	S+_ppm	O_wt%	Co_ppm	Ni_ppm	Cu_ppm	Rb_ppm	Sr_ppm	Ba_ppm	Yb_ppm		
Cumulate	18.63	0.03	0.06	0.00	8.69	0.15	28.26	0.20	0.00	0.00		0.03	4.4	2937.3	631.8	6.7	43.337	169.4	2287.1	269.7	0.0	0.9	0.0			
	SiO2	TiO2	Al2O3	Fe2O3	FeO	MnO	MgO	CaO	Na2O	K2O	P2O5	Cr2O3	FeS*_ppm	H2O_wt%	CO2_ppm	S_ppm	S03_ppm	O_wt%	Co_ppm	Ni_ppm	Cu_ppm	Rb_ppm	Sr_ppm	Ba_ppm	Yb_ppm	
Olv	40.37	0.04	0.11	0.00	11.23	0.20	47.46	0.28	0.00	0.00		0.04						0.057	166.4	1920.3		0.0	0.9			
	SiO2	TiO2	Al2O3	Fe2O3	FeO	MnO	MgO	CaO	Na2O	K2O	P2O5	Cr2O3		H2O_wt%	CO2_ppm	H2S_ppm	S02_ppm	O_wt%	Co_ppm	Ni_ppm	Cu_ppm	Rb_ppm	Sr_ppm	Ba_ppm	Yb_ppm	
Fld														0.361	995028.9	101.2	1245.2	0.000				1.8	8.5	0.9		
	SiS2	TiS2	Al2S3	Fe2S3	FeS	MnS	MgS	CaS	Na2S	K2S	P2S5	Cr2S3	FeO_ppm	H2O_wt%	CO2_ppm	S_ppm	S03_ppm	O_wt%	Co_ppm	Ni_ppm	Cu_ppm	Rb_ppm	Sr_ppm	Ba_ppm	Yb_ppm	
Slf					47.85								42224.4			143475.4		2567.1	197311.3	135962.6						
Fo= 88.277; Fe#Slf= 64.205; CO2#Fl= 98.231; Amounts (wt%) of cumulate phases: Olv 1.5682; Slf 0.0032; Fld 0.01718;																										

Output using elemental concentrations

	Si	Ti	Al	Fe3	Fe2	Mn	Mg	Ca	Na	K	P	Cr	H_ppm	C+_ppm	S-_ppm	S+_ppm	O_wt%	Co_ppm	Ni_ppm	Cu_ppm	Rb_ppm	Sr_ppm	Ba_ppm	Yb_ppm
Magma	23.43	0.78	8.43	0.70	6.05	0.14	6.15	7.11	1.26	0.58	0.05	0.07	580.9	899.5	837.8	1.3	44.989	52.0	162.2	145.0	9.0	85.6	3.0	10.0
Melt	23.45	0.78	8.46	0.70	6.04	0.14	6.06	7.14	1.26	0.58	0.05	0.07	583.3	855.7	831.1	1.2	44.993	51.5	150.1	141.0	9.0	85.9	3.0	10.0
Olv	18.85	0.03	0.06	0.00	8.91	0.16	28.51	0.21	0.00	0.00		0.03						168.4	1746.0		0.0	0.9		
Slf					34.99													1.003	2612.2	180124.9	141095.4			
Fld													433.4	271423.0	100.3	711.2	72.732				1.8	8.6	0.9	
Fo= 88.025 Kd(Olv-Melt)= 0.314; Fe#Slf= 67.122; CO2#Fl= 99.064; T=1213.3 (Olv); Lg(fO2)=-8.52 dQFM=-0.73; TPlg=1115.8 TCpx=1154.9 T0px=1191.4 TPig=1167.7 Amounts (wt%) of phases in magma: Melt 97.9991; Olv 0.3920; Slf 0.0032; Fld 0.01718; Pressure: 4.800 kbar; Density: 2.677 g/cm3; Viscosity: v=26 poise; ln(v)=3.2																								
	Si	Ti	Al	Fe3	Fe2	Mn	Mg	Ca	Na	K	P	Cr	H_ppm	C+_ppm	S-_ppm	S+_ppm	O_wt%	Co_ppm	Ni_ppm	Cu_ppm	Rb_ppm	Sr_ppm	Ba_ppm	Yb_ppm
Cumulate	18.63	0.03	0.06	0.00	8.69	0.15	28.26	0.20	0.00	0.00		0.03	4.4	2937.3	631.8	6.7	43.337	169.4	2287.1	269.7	0.0	0.9	0.0	
Olv	18.87	0.03	0.06	0.00	8.73	0.15	28.62	0.20	0.00	0.00		0.03						166.4	1920.3		0.0	0.9		
Slf					33.68													0.940	2567.1	197311.3	135962.6			
Fld													407.2	271535.9	95.3	623.2	72.733				1.8	8.5	0.9	
Fo= 88.277; Fe#Slf= 64.205; CO2#Fl= 98.231; Amounts (wt%) of cumulate phases: Olv 1.5682; Slf 0.0032; Fld 0.01718;																								

Note: When output using components is chosen, the magma composition in this example is shown using the elemental concentration. This is because when fluid and / or immiscible sulphide melt are present in the magma, it impossible to display the combined composition of all phases in the magma using components. When neither fluid nor sulphide are present in the magma, its composition is shown using components.

Note: When fluid and / or immiscible sulphide melt are present among fractionated phases, the bulk composition of the ‘Cumulate’ is shown using elemental concentration even if the output using component concentrations is chosen. This is because in such a case it is impossible to display the combined composition of fractionated phases (the ‘Cumulate’ composition) using components. When neither fluid nor sulphide are present, the composition of the ‘Cumulate’ is shown using components when the output using component concentrations is chosen.

Table 4.4. Example output: An intermediate state of the system during calculations at 40% of crystallisation of the starting composition (Tables 4.1, 4.2)

Output using component concentrations

	Si	Ti	Al	Fe3	Fe2	Mn	Mg	Ca	Na	K	P	Cr	H_ppm	C+_ppm	S-_ppm	S+_ppm	O_wt%	Co_ppm	Ni_ppm	Cu_ppm	Rb_ppm	Sr_ppm	Ba_ppm	Yb_ppm		
Magma	24.29	1.02	8.68	0.87	6.20	0.15	3.80	7.17	1.45	0.76	0.06	0.09	764.6	629.1	891.5	18.2	45.168	41.3	42.4	105.8	11.7	94.2	3.9	12.7		
	SiO2	TiO2	Al2O3	Fe2O3	FeO	MnO	MgO	CaO	Na2O	K2O	P2O5	Cr2O3	FeS*_ppm	H2O_wt%	CO2_ppm	S_ppm	SO3_ppm	O_wt%	Co_ppm	Ni_ppm	Cu_ppm	Rb_ppm	Sr_ppm	Ba_ppm	Yb_ppm	
Melt	53.29	2.11	14.99	1.49	8.50	0.22	5.32	9.48	1.99	1.14	0.18	0.16	2300.2	0.831	249.4		21.1	0.004	37.8	13.1	49.2	14.2	90.1	4.6	15.5	
Plg	49.07		32.34	0.35	0.22			15.25	2.76									0.003				1.4	164.8	0.9		
Olv	39.02	0.07	0.11	0.00	18.16	0.40	41.66	0.41	0.00	0.00		0.10						0.014	216.0	286.5		0.0	0.9			
Cpx	50.93		6.05		8.20		16.11	18.71										0.001	7.6	13.2		0.7	6.3	0.1	10.6	
	SiO2	TiO2	Al2O3	Fe2O3	FeO	MnO	MgO	CaO	Na2O	K2O	P2O5	Cr2O3		H2O_wt%	CO2_ppm	H2S_ppm	SO2_ppm	O_wt%	Co_ppm	Ni_ppm	Cu_ppm	Rb_ppm	Sr_ppm	Ba_ppm	Yb_ppm	
Fld														8.012	907600.3	2454.7	9805.0	0.000				2.8	9.0	1.4		
	SiS2	TiS2	Al2S3	Fe2S3	FeS	MnS	MgS	CaS	Na2S	K2S	P2S5	Cr2S3	FeO_ppm	H2O_wt%	CO2_ppm	S_ppm	SO3_ppm	O_wt%	Co_ppm	Ni_ppm	Cu_ppm	Rb_ppm	Sr_ppm	Ba_ppm	Yb_ppm	
Slf					74.19								84027.7			42756.0			2895.3	29855.5	98603.6					
An= 75.351; Fo= 80.349 Kd(Olv-Melt)= 0.267; Mg#Cpx= 77.787; Fe#Slf= 94.972; CO2#Fl= 82.247; T=1058.0 (Plg); Lg(fO2)=-9.75 dQFM=0.31; Tolv=1058.0 TCpx=1058.0 TOpx=1040.1 TPig=1047.3 TMgt=988.0																										
Amounts (wt%) of phases in magma: Melt 59.9944; Olv 2.9942; Plg 9.6513; Cpx 1.5860; Slf 0.0499; Fld 0.17262; Pressure: 0.666 kbar; Density: 2.666 g/cm3; Viscosity: v=60 poise; ln(v)=4.1																										
	Si	Ti	Al	Fe3	Fe2	Mn	Mg	Ca	Na	K	P	Cr	H_ppm	C+_ppm	S-_ppm	S+_ppm	O_wt%	Co_ppm	Ni_ppm	Cu_ppm	Rb_ppm	Sr_ppm	Ba_ppm	Yb_ppm		
Cumulate	20.63	0.01	7.16	0.08	5.83	0.09	14.35	6.51	0.60	0.00		0.02	9.7	1813.9	610.3	10.4	44.364	90.6	643.2	266.9	0.5	55.3	0.3	1.4		
	SiO2	TiO2	Al2O3	Fe2O3	FeO	MnO	MgO	CaO	Na2O	K2O	P2O5	Cr2O3	FeS*_ppm	H2O_wt%	CO2_ppm	S_ppm	SO3_ppm	O_wt%	Co_ppm	Ni_ppm	Cu_ppm	Rb_ppm	Sr_ppm	Ba_ppm	Yb_ppm	
Olv	39.98	0.05	0.10	0.00	13.34	0.25	45.73	0.35	0.00	0.00		0.06						0.033	179.5	1029.9		0.0	0.9			
Plg	47.73		33.30	0.29	0.19			16.34	2.13									0.003				1.1	142.7	0.6		
Cpx	50.92		6.30		7.36		16.27	19.14										0.001	7.5	15.8		0.7	6.3	0.1	9.4	
	SiO2	TiO2	Al2O3	Fe2O3	FeO	MnO	MgO	CaO	Na2O	K2O	P2O5	Cr2O3		H2O_wt%	CO2_ppm	H2S_ppm	SO2_ppm	O_wt%	Co_ppm	Ni_ppm	Cu_ppm	Rb_ppm	Sr_ppm	Ba_ppm	Yb_ppm	
Fld														1.267	983880.0	364.2	3076.7	0.000				2.1	9.0	1.0		
	SiS2	TiS2	Al2S3	Fe2S3	FeS	MnS	MgS	CaS	Na2S	K2S	P2S5	Cr2S3	FeO_ppm	H2O_wt%	CO2_ppm	S_ppm	SO3_ppm	O_wt%	Co_ppm	Ni_ppm	Cu_ppm	Rb_ppm	Sr_ppm	Ba_ppm	Yb_ppm	
Slf					63.32								66424.2			80139.5			2757.9	80910.5	136539.1					
Fo= 85.939; An= 80.922; Mg#Cpx= 79.763; Fe#Slf= 85.498; CO2#Fl= 93.993; Amounts (wt%) of cumulate phases: Olv 11.9769; Plg 9.6513; Cpx 3.7007; Slf 0.0499; Fld 0.17262;																										

Output using elemental concentrations

	Si	Ti	Al	Fe3	Fe2	Mn	Mg	Ca	Na	K	P	Cr	H_ppm	C+_ppm	S-_ppm	S+_ppm	O_wt%	Co_ppm	Ni_ppm	Cu_ppm	Rb_ppm	Sr_ppm	Ba_ppm	Yb_ppm		
Magma	24.29	1.02	8.68	0.87	6.20	0.15	3.80	7.17	1.45	0.76	0.06	0.09	764.6	629.1	891.5	18.2	45.168	41.3	42.4	105.8	11.7	94.2	3.9	12.7		
Melt	24.91	1.26	7.93	1.04	6.75	0.17	3.21	6.78	1.48	0.95	0.08	0.11	922.8	68.0	838.9	8.4	45.113	37.8	13.1	49.2	14.2	90.1	4.6	15.5		
Plg	22.94		17.11	0.25	0.17			10.90	2.04								46.574				1.4	164.8	0.9			
Olv	18.24	0.04	0.06	0.00	14.12	0.31	25.13	0.30	0.00	0.00		0.07					41.695	216.0	286.5		0.0	0.9				
Cpx	23.81		3.20		6.38		9.72	13.37									43.527	7.6	13.2		0.7	6.3	0.1	10.6		
Slf					53.66												1.871	2895.3	29855.5	98603.6						
Fld													9046.9	247677.3		313306.5	2310.5	4907.1	73.604		2.8	9.0	1.4			
An= 75.351; Fo= 80.349 Kd(Olv-Melt)= 0.267; Mg#Cpx= 77.787; Fe#Slf= 94.972; CO2#Fl= 82.247; T=1058.0 (Plg); Lg(fO2)=-9.75 dQFM=0.31; Tolv=1058.0 TCpx=1058.0 TOpx=1040.1 TPig=1047.3 TMgt=988.0 Amounts (wt%) of phases in magma: Melt 59.9944; Olv 2.9942; Plg 9.6513; Cpx 1.5860; Slf 0.0499; Fld 0.17262; Pressure: 0.666 kbar; Density: 2.666 g/cm3; Viscosity: v=60 poise; ln(v)=4.1																										
	Si	Ti	Al	Fe3	Fe2	Mn	Mg	Ca	Na	K	P	Cr	H_ppm	C+_ppm	S-_ppm	S+_ppm	O_wt%	Co_ppm	Ni_ppm	Cu_ppm	Rb_ppm	Sr_ppm	Ba_ppm	Yb_ppm		
Cumulate	20.63	0.01	7.16	0.08	5.83	0.09	14.35	6.51	0.60	0.00		0.02	9.7	1813.9	610.3	10.4	44.364	90.6	643.2	266.9	0.5	55.3	0.3	1.4		
Olv	18.69	0.03	0.05	0.00	10.37	0.19	27.58	0.25	0.00	0.00		0.04						42.683	179.5	1029.9		0.0	0.9			
Plg	22.31		17.62	0.20	0.15			11.68	1.58									46.440				1.1	142.7	0.6		
Cpx	23.81		3.33		5.72		9.81	13.68										43.643	7.5	15.8		0.7	6.3	0.1	9.4	
Slf					45.39													1.479	2757.9	80910.5	136539.1					
Fld													1428.6	268493.5		342.8	1539.8	72.818				2.1	9.0	1.0		
Fo= 85.939; An= 80.922; Mg#Cpx= 79.763; Fe#Slf= 85.498; CO2#Fl= 93.993; Amounts (wt%) of cumulate phases: Olv 11.9769; Plg 9.6513; Cpx 3.7007; Slf 0.0499; Fld 0.17262;																										

4.1.10. Setting conditions to stop calculations

Petrolog4 offers several options for defining conditions for stopping calculations. The default setting is 0 wt.% of crystallisation, indicating that no crystallisation calculation is performed. To change this setting, click on the blue text label below 'Define conditions to stop calculations:' text label inside the 'Calculation Parameters' sub-section in the Parameters Section (Figs. 1.1, 1.2, 2.2). The 'Conditions for stopping calculations' window will pop-up (Fig. 4.18). The user must choose one of the available options.

Close the window by pressing the 'Ok' button. Pressing the 'Cancel' button closes the window without applying the changes made. The blue label will display the chosen option.

Figure 4.18. The 'Conditions for stopping calculation' window showing options available for setting conditions for stopping calculations.

Note: The data file can contain columns that contain conditions to stop calculations that can differ for each analysis. Such columns should have the following name in the header row: LASTFRAC or LAST_FRAC, LASTTEMP or LAST_TEMP, LASTMGO or LAST_MGO, LASTFO or LAST_FO, LASTAN or LAST_AN, LASTCPX or LAST_CPX, LASTOPX or LAST_OPX, LASTPIG or LAST_PIG corresponding to the options shown on Fig. 4.18. The parameters should be in the same units as shown on Fig. 4.18.

4.1.11. Setting conditions for modelling replenishment

Petrolog4 algorithm allows for modelling replenishment of the crystallising system by the parental melt during pure fractional crystallisation. Replenishment involves repeated instances of recharge of the crystallising system by the parental melt (i.e., by a melt of the same composition as the starting composition), and optional linked instances of eruptions of the evolved melt from the crystallising system. When Petrolog4 starts, replenishment is not chosen. To set replenishment parameters click on one of the three blue labels ('Recharge...', 'Eruption...' or 'Trigger...') in the 'Replenishment parameters' subsection of the Parameters Section of the Main form (Figs. 1.1, 1.2, 2.2).

Figure 4.19. The 'Replenishment Settings' window showing options available for setting conditions for the primitive melt recharge and evolved melt eruption during calculations.

Clicking on any of the three blue labels opens the Replenishment Settings form (Fig. 4.19).

Note: Since replenishment is only enabled for the case of pure fractional crystallisation, if the extent of fractionation is set to less than 100 for any of the phases (see section 4.1.2), the 'Replenishment parameters' subsection is disabled (Fig. 1.2).

The mass of the recharge and eruption events is set separately as a percentage of the mass of the melt present in the crystallising system. (Fig. 4.19). If the percentage of the erupted melt is lower than the recharge, the mass of the crystallising system increases with each recharge. Conversely, if the mass of the erupted melt exceeds the mass of the recharge, the mass of the crystallising system continuously decreases during calculations. Petrolog4 algorithm places eruption events immediately prior to recharge events, i.e., there is

always the same number of eruption and recharge events.

To enable replenishment calculations, the user also needs to specify the trigger for recharge events (Fig. 4.19). Petrolog4 offers a choice of three triggers:

- 1) when a specified proportion of crystals is formed after the beginning of calculations or after the previous recharge instance. This trigger option allows the composition of the melt inside the crystallising system to continuously evolve towards more fractionated compositions;
- 2) when the proportion of melt in the crystallising system reaches a set value. Using this trigger requires that the proportion of recharge is larger than the proportion of the erupted melt. This trigger will maintain the proportion of melt in the crystallising system near the set value, resulting a steady-state-like scenario when the major element compositions of the erupted melts will be similar;
- 3) when the MgO content in the melt reaches a set value. In most cases this trigger requires that the set value for the MgO content in the melt is lower than the MgO content in the starting composition. Similarly to the second trigger, a steady-state-like scenario will occur resulting in similar major element compositions of the erupted melts.

When replenishment is included in calculations, each recharge event triggers output of the state of the system immediately after the recharge, and the composition of the erupted melt is recorded immediately prior to recharge. Petrolog4 output contains values for the number of recharge events that occurred from the beginning of calculation; the current mass of the crystallising system relative to the initial mass; the current mass of the erupted melt relative to the initial mass, and the current mass of recharge relative to the initial mass.

4.2. Saving and loading calculation parameters

To save the current set of calculation parameters, use the 'Save Parameters' option in the 'File' section of the Main Menu on the Main form (Fig. 2.2). In the dialog form that appears, enter a file name and press Save.

Note: Petrolog4 assigns .PtlParam extension to files with parameter values.

Petrolog4 offers options to include the names of either the data file or the file with the saved D values, or both, in the parameters file. To set these two options, use the 'Petrolog Options' form that is opened by choosing the 'Options' item in the 'Tools' section of the Main Menu (Fig. 2.4)

Note: When planning to pass on files with parameters to other users, before saving the parameters file, deselect options for including the names of the data file and the file with the saved D values in the parameters file.

To load a previously saved set of calculation parameters, use the 'Load Parameters' option in the 'File' section of the Main Menu on the Main form (Fig. 2.2). Choose the file in the dialog window and press Open.

4.2.1. Saving the Default Set of calculation parameters.

To save the current set of calculation parameters as the Default Set, use the 'Save Parameters as the Default Set' option in the 'File' section of the Main Menu on the Main form (Fig. 2.2). Once saved, this set of parameters will be loaded every time Petrolog4 starts. To reload this set of parameters while using Petrolog4, use 'Load the Default Set of Parameters' option in the 'File' section of the Main Menu on the Main form (Fig. 2.2).

Note: The Program Default set of parameters can be restored by using the 'Reset Program Defaults' option of the Tools Menu (Fig. 1.2).

4.3. Structure of output files

During modelling of crystallisation, Petrolog4 saves the following files:

FileName_FRAC__calc_param.csv file lists values of all calculation parameters.

FileName_FRAC__.csv file contains:

- magma, melt and bulk cumulate compositions;
- proportions of all phases in the magma and cumulate;

compositional parameters of phases crystallising from the magma;
compositional parameters of the bulk phases in the cumulate;
temperature, pressure and melt physical properties.

Compositions of each phase in equilibrium with the melt at each recorded stage of fractionation are saved in a separate file. Such files have the following names:

FileName_FRAC_Olv_MAG.csv for olivine compositions;
FileName_FRAC_Plg_MAG.csv for plagioclase compositions;
FileName_FRAC_Cpx_MAG.csv for clinopyroxene compositions;
FileName_FRAC_Opx_MAG.csv for orthopyroxene compositions;
FileName_FRAC_Pig_MAG.csv for pigeonite compositions;
FileName_FRAC_Spl_MAG.csv for spinel compositions;
FileName_FRAC_Ilmen_MAG.csv for ilmenite compositions;
FileName_FRAC_Mgt_MAG.csv for magnetite compositions;
FileName_FRAC_Slf_MAG.csv for sulphide compositions;
FileName_FRAC_Fld_MAG.csv for fluid compositions;
FileName_FRAC_Qtz_MAG.csv for quartz compositions;
FileName_FRAC_Ort_MAG.csv for orthoclase compositions;
FileName_FRAC_Nph_MAG.csv for nepheline compositions;
FileName_FRAC_Lct_MAG.csv for leucite compositions.
FileName_FRAC_Zrn_MAG.csv for zircon compositions.
FileName_FRAC_Apt_MAG.csv for apatite compositions.
FileName_FRAC_Erupt_Melt.csv for compositions of the erupted melt.

Note: When 'Add export of elemental concentrations to files' option is used (see Section 1.2), an additional set of files with phase compositions will be added that have '_EL' added at the end of their names (e.g., FileName_FRAC__EL.csv, FileName_FRAC_Plg_MAG_EL.csv, etc.).

Note: When 'Add export of cumulus phases to files' option is used (see Section 1.2), an additional set of files with phase compositions will be added that have '_CUM' added at the end of their names instead of 'MAG' (e.g., FileName_FRAC_Plg_CUM.csv, FileName_FRAC_Plg_CUM_EL.csv, etc.).

Note: Files that are saved during each calculation are only for those phases that have appeared on the liquidus during calculations.

Note: When exporting results of previous calculations to Excel, the user must click on the FileName_FRAC__.csv file to initiate export.

Note: When using user-defined file names, it is recommended to keep file names under 15 characters long, since the length of allowed names for individual sheets in Excel files is limited to 31 characters.

5. Melt liquidus association

To determine melt liquidus association, choose 'Melt liquidus association' tab of the Main form (Fig. 5.1).

Petrolog 4.2.2 Input from: C:\Programs\Delphi\Petrolog4\Manual\Current_data_File.csv Memory Usage: 1.908 Mb

File Export to MS Excel Tools Help

Crystallisation Reverse Crystallisation **Melt Liquidus Association** Olivine MI

Choose models for phases
☐ Select All ☐ Deselect All
 Olivine
☒ Ford et al. 1983
☐ Putirka et al. 2007
☐ Herzberg & O'Hara 2002
☒ Danyushevsky 2001
☐ Ariskin et al. 1993
☒ Beattie 1993
☐ Langmuir et al. 1992
☐ Weaver & Langmuir 1990
☐ Putirka et al. 2008
☐ Putirka 2005 (C-D)
☐ Putirka 2005 (A-B)
☐ Gaetani & Watson 2002

Corrections for models:

Mineral	P	W
Olivine		
Plagioclase		
Clinopyroxene		
Orthopyroxene		
Pigeonite		
Spinel		
Ilmenite		
Magnetite	c	c
Sulphide	n/a	n/a
Fluid	n/a	n/a

Oxidation state:
 Calculations performed using:
[Oxygen Buffer: 'QFM'](#)
[Change Oxidation models:](#)
 Model for Fe: Borisov et al 2018
 Model for S: O'Neill & Mavrogenes 2022

Saturation Models:
[Change Saturation Models:](#)
 Sulfide: Fortin et al. 2015
 Fluid: Iacono-Marziano et al 2012
 Sulfate: Zajacz & Tsay 2019
 Apatite: Tollari et al. 2006
 Zircon: Crisp & Berry 2022

Pressure:
 P (kbar): 0.1

Starting melt composition

SiO2	TiO2	Al2O3	Fe2O3	FeO	MnO	MgO	CaO	Na2O	K2O	P2O5	Cr2O3	H2O
48.00	1.00	14.00	0.50	9.00	0.16	7.00	9.00	2.00	0.20	0.22	0.08	0.00

Analysis1 ☒ Calculate all analyses [Select another analysis](#) [Set volatile and trace elements*](#)

Output to: Ptl_Oltp_*.csv D values: loaded from Ds_fractionation_250214_v411.PtlDSet

Parameters: last loaded from S_in_glass_calc.PtlParam modified

Start calculations **Clear Results** Follow output: ☐ On

Analysis1

	SiO2	TiO2	Al2O3	Fe2O3	FeO	MnO	MgO	CaO	Na2O	K2O	P2O5	Cr2O3	FeS*_ppm	H2O_wt%	CO2_ppm	S_ppm	SO3_ppm	Cl_ppm	O_wt%	Co_ppm	Ni_ppm	Rb_ppm	Sr_ppm	Ba_ppm
Olv	50.16	1.28	15.74	1.22	7.65	0.18	10.82	9.84	1.67	0.69	0.11	0.11		0.492	0.0		0.0	60.0	0.006	54.1	71.8	8.9	84.6	66.9
Olv													Mgt											
Ford83	Danyus01	Beatt93	Danyus01	Arisk93	Langm92	Danyus01	Arisk93	Langm92	Arisk99															
1267.3	1289.4	1263.3	1095.6	1173.4	1195.1	1144.6	1190.3	1171.0	982.7															
Fo	Fo	Fo	An	An	An	Mg#Cpx	Mg#Cpx	Mg#Cpx	Mg#Mgt															
88.82	88.82	89.18	85.34	81.03	82.88	90.08	90.10	90.20	47.44															

Could not estimate cotectic melt H2O content because Tol > Tpl. Melt H2O content was not changed.
 Estimated Pressure for an Oliv-Cpx cotectic = 11.916 kbar.
 Saturation pressure (kbar): Moore et al. 1998: 0.040; Newman & Lowenstern 2002: 0.024; Iacono-Marziano et al 2012: 0.033; Shishkina et al. 2014 (H2O): 0.017; Shishkina et al. 2014 (CO2): 0.001;

Analysis3

	SiO2	TiO2	Al2O3	Fe2O3	FeO	MnO	MgO	CaO	Na2O	K2O	P2O5	Cr2O3	FeS*_ppm	H2O_wt%	CO2_ppm	S_ppm	SO3_ppm	Cl_ppm	O_wt%	Co_ppm	Ni_ppm	Rb_ppm	Sr_ppm	Ba_ppm
Olv	48.12	0.80	14.04	1.86	9.85	0.20	9.02	13.03	2.01	0.60	0.24	0.13	545.0	0.000	0.0		4.4	36.1	0.006	50.1	88.2	15.0	54.1	55.1
Olv																								
Ford83	Danyus01	Beatt93	Danyus01	Arisk93	Langm92	Danyus01	Arisk93	Langm92	Arisk99															
1214.9	1214.9	1224.6	1176.6	1186.8	1169.1	1193.2	1186.1	1223.0	1044.7															
Fo	Fo	Fo	An	An	An	Mg#Cpx	Mg#Cpx	Mg#Cpx	Mg#Mgt															
83.92	83.92	84.20	76.09	76.47	77.61	85.35	85.38	85.36	35.30															

Could not estimate cotectic melt H2O content because Tol > Tpl. Melt H2O content was not changed.
 Estimated Pressure for an Oliv-Cpx cotectic = 4.058 kbar

Figure 5.1. 'Melt Liquidus Association' option of Petrolog4 interface.

Note: It is recommended that you read Section 4 of this Manual before reading this section.

In this option, Petrolog4 does not model a crystallisation path but calculates pseudo-liquidus temperatures and liquidus phase compositions for a chosen set of phases and phase-melt equilibrium models. The following phase compositional parameters are also calculated:

Olivine:

Plagioclase:

Clinopyroxene; Orthopyroxene; Pigeonite; Ilmenite and Magnetite:

Spinel:

Sulphide:

Fluid (mol units):

Sulphate:

Quartz:

Orthoclase; Leucite:

Nepheline:

Zircon:

Apatite:

mol% forsterite (Fo);

mol% anorthite (An);

Mg# ($100 \cdot \text{Mg} / (\text{Mg} + \text{Fe})$);

Cr# ($100 \cdot \text{Cr} / (\text{Cr} + \text{Al})$);

Fe# ($100 \cdot \text{Fe} / (\text{Fe} + \text{Ni})$);

CO2# ($100 \cdot \text{CO}_2 / (\text{CO}_2 + \text{H}_2\text{O})$).

Ca# ($100 \cdot \text{Ca} / (\text{Ca} + \text{Ba})$);

Si# ($100 \cdot \text{Si} / (\text{Si} + \text{Al})$);

K# ($100 \cdot \text{K} / (\text{K} + \text{Na})$);

Na# ($100 \cdot \text{Na} / (\text{K} + \text{Na})$);

Hf# ($100 \cdot \text{Hf} / (\text{Hf} + \text{Zr})$);

Ca# ($100 \cdot \text{Ca} / (\text{Ca} + \text{Sr} + \text{Ba} + \text{REE})$).

By comparing calculated temperatures for different phases, the liquidus association of a melt composition can be established according to the chosen phase-melt equilibrium models. As the stated errors for most

models are ~ 15 - 20 °C, the liquidus association would include the phase(s) with the highest calculated temperature (i.e., the liquidus temperature) and phases which pseudo-liquidus temperatures are within ~ 20 °C of the calculated liquidus temperature.

Note: During melt liquidus association calculations it is possible to choose any number of models for each phase. This allows a comparison to be made between different models.

Corrections to the calculated liquidus temperatures for the effects of pressure and melt H₂O contents are set in the 'Correction for models:' subsection of the Parameters Section of the Main form (Fig. 5.1) in the same way as for Crystallisation calculations (see sections 4.1.1.2 and 4.1.1.3).

Note: The same correction will apply to all models selected for a phase. If a selected model incorporates the effects of pressure and/or H₂O, then the option 'Apply H₂O and P Corrections to All Models' (see Section 1.2) defines whether the correction(s) will apply to that model. When the option is selected, the correction(s) will apply to models that incorporate the effects of pressure and/or H₂O.

If the H₂O and / or CO₂ contents in the starting composition(s) exceed fluid saturation values for the chosen pressure, their concentrations will be adjusted to match saturation at the chosen pressure before temperatures are calculated.

If the S content in the starting composition(s) exceeds sulphide or sulphate saturation, S concentrations will be adjusted to match saturation before temperatures are calculated.

Note: If the starting composition is sulphide, sulphate, zircon, apatite or fluid saturated, the established liquidus temperature is assigned to these phases and used for calculating their compositions.

Note: The oxidation states of Fe and S in the melt composition recorded in the results output correspond to the established liquidus temperature (i.e., the highest calculated temperature among the models chosen for calculation).

When models of Danyushevsky (2001) for olivine AND plagioclase are chosen, Petrolog4 automatically estimates the H₂O content in the melt which is required for the starting composition to lie on an olivine + plagioclase cotectic. The estimated H₂O content is reported for each composition below the line with mineral compositional parameters (Fig. 5.1).

When models of Danyushevsky (2001) for olivine AND clinopyroxene are chosen, Petrolog4 automatically estimates crystallisation pressure at which the starting composition has both olivine and clinopyroxene on its liquidus. The estimated crystallisation pressure is reported for each composition below the line with mineral compositional parameters (Fig. 5.1).

Note: Models of Danyushevsky (2001) are calibrated for MORB and BABB compositions only and should not be used for calculations with compositions from other tectonic settings.

If the starting composition contains either H₂O or CO₂ or both, Petrolog4 automatically estimates fluid saturation pressures for the starting composition using all available models of fluid saturation that are applicable to the silicate melt compositions involved (i.e., whether the compositions contain both H₂O and CO₂, only H₂O, or only CO₂). The estimated fluid saturation pressure is reported for each composition below the line with mineral compositional parameters (Fig. 5.1). 'N/A' is displayed for the fluid saturation models that are not applicable.

Note: If the starting composition is fluid-oversaturated relative to the pressure chosen for calculations, the saturation pressure will be calculated for the unmodified starting composition before its volatile contents are adjusted to reflect saturation at the pressure chosen for calculation. Since calculations of the saturation pressure involve melt liquidus temperature, it is recommended that the calculation pressure is set above the saturation pressure of the starting composition(s) to ensure that the calculated liquidus temperature is appropriate for the volatile contents of the starting composition.

Since crystallisation calculations are not performed under this Option, the number of calculation parameters that can be set by the user is significantly less compared to Crystallisation calculations.

Fluid, sulphur, apatite and zircon saturation models are set in the 'Saturation models:' subsection of the Parameters Section of the Main form (Fig. 5.1) in the same way as for Crystallisation calculations (see section 4.1.4).

Melt oxidation state is set in the 'Oxidation state' subsection of the Parameters Section of the Main form (Fig. 5.1) in the same way as for Crystallisation calculations (see section 4.1.5).

Pressure is set in the 'Pressure' subsection of the Parameters Section of the Main form (Fig. 5.1). It is possible to load pressure values to be used in calculations from the data file with analyses. Those values can differ for each analysis (see Section 4.1.3 for details).

Note: If you would like to use additional options for calculating minerals compositions (see sections 4.1.1.1a and 4.1.1.1b), you should choose them in the Crystallisation tab as described in Section 4.

5.1. Saving and loading calculation parameters and structure of output files

Saving and Loading calculation parameters is done in the same way as for Crystallisation calculations (see section 4.2).

During melt liquidus association calculations, Petrolog4 saves the following files:

FileName_MLA__calc_param.csv file lists values of all calculation parameters.

FileName_MLA__.csv file contains the starting melt composition, and pseudo-liquidus temperatures and compositional parameters of phases for the selected models.

Note: When exporting results of previous calculations to Excel, the user must click on the FileName_MLA__.csv file to initiate export.

Compositions of each phase in equilibrium with the melt are saved in a separate file that have the same naming convention as for Crystallisation calculations (e.g., file FileName_MLA_Olv.csv contains olivine compositions).

Note: When 'Add export of elemental concentrations to files' option is used (see Section 1.2), an additional set of files with phase compositions will be added that have '_EL' added at the end of their names (e.g., FileName_MLA__EL.csv, FileName_MLA_Plg_EL.csv, etc.).

Note: When using user-defined file names, it is recommended to keep file names under 15 characters long, since the length of allowed names for individual sheets in Excel files is limited to 31 characters.

6. Reverse of fractional crystallisation

To model reverse of fractional crystallisation, choose 'Reverse Crystallisation' tab of the Main form (Fig. 6.1).

Petrolog 4.2.2 Input from: C:\Programs\Petrolog4\DemoFiles\Current_data_File.csv Memory Usage: 1.982 Mb

File Export to MS Excel Tools Help

Crystallisation Reverse Crystallisation Melt Liquidus Association Olivine MI

Models for phase-melt equilibrium:

Phase	Model	P	W	Tr
Olivine	Herzberg & O'Hara 2002	Y	c	Y
Plagioclase	Ariskin et al. 1993	Y	c	
Clinopyroxene	Weaver & Langmuir 1990		c	
Orthopyroxene	Bolkhovskaya et al. 1996	Y	c	
Pigeonite	Bolkhovskaya et al. 1996	Y	c	
Spinel	Ariskin & Nikolaev 1996		c	
Ilmenite	Press to Select			
Magnetite	Ariskin & Barmina 1999		c	
Sulfide	Press to Select			
Fluid	VolatileCalc 2002	Y	Yc	

☐ Force Pl-Ol cotectic (for MORB and BABB only)

Parameters for exclusion:

Plagioclase [Fo limit\(s\)](#)
 Orthopyroxene [press to set](#)
 Clinopyroxene [Mg limit\(s\)](#)
 Pigeonite [Comp limit\(s\)](#)
 Magnetite [press to set](#)
 Ilmenite [press to set](#)
 Sulfide [Mg limit\(s\)](#)
 Fluid [T limit\(s\)](#)
 Sulfate [press to set](#)
 Quartz [press to set](#)
 Orthoclase [press to set](#)
 Nepheline [press to set](#)
 Leucite [press to set](#)
 Zircon [press to set](#)
 Apatite [press to set](#)

Oxidation state:
 Calculations performed using:
[Closed system for Oxygen](#)
[Change Oxidation Models:](#)
 Model for Fe: Borisov et al 2018
 Model for S: O'Neill & Mavrogenes 2002

Melt physical properties:
 Density: [Lange & Carmichael 1987](#)
 Viscosity: [Giordano & Dingwell 2003](#)

Calculation parameters:
 Calculation step: %
 Define output frequency:
[Crystallisation step = 1.0 %](#)
 A total of 1 output condition(s) chosen
 Define conditions to stop calculations:
[Melt MgO content = 12 wt%](#)

Pressure:
 Initial P (kbar):
 Set Pressure behaviour:
[Keep constant](#)

Saturation Models:
[Change Saturation Models:](#)
 Sulfide: O'Neill 2021
 Fluid: Newman & Lowenstern 2002
 Sulfate: Zajacz & Tsay 2019
 Apatite: Tollari et al. 2006
 Zircon: Crisp & Berry 2022

Starting melt composition:

SiO2	TiO2	Al2O3	Fe2O3	FeO	MnO	MgO	CaO	Na2O	K2O	P2O5	Cr2O3	H2O
48.00	1.30	13.00	0.90	8.00	0.23	7.00	10.00	2.40	1.60	0.18	0.13	0.00

☐ Fluid saturated ☐ Sulfide saturated
[Set volatile and trace elements*](#)

Analysis4 ☐ Calculate all analyses [Select another analysis](#)

Output to: Ptl_Otpt_*.csv D Values: modified in this session

Parameters: last loaded from Tables4.PtlParam modified

Start calculations **Clear Results** Follow output: ☐ On

Melt viscosity is calculated following the model of Giordano & Dingwell 2003
 Parameters for excluding Plagioclase from calculations:
 Upper Fo limit for Plagioclase: 90 mol%
 Parameters for excluding Clinopyroxene from calculations:
 Max melt MgO content for Clinopyroxene: 9 wt%
 Parameters for excluding Pigeonite from calculations:
 Upper compositional limit for Pigeonite: 90 mol%
 Parameters for excluding Sulfide from calculations:
 Max melt MgO content for Sulfide: 9 wt%
 Parameters for excluding Fluid from calculations:
 Upper temperature limit for Fluid: 1200(C)
 Parameters to stop calculations at:
 Final melt MgO content: 12 wt%
 The amount of a mineral phase which will be added to
 100% of melt on each step is: 0.01 %

The starting composition "Analysis4" has been adjusted for the chosen oxidation state, checked for fluid, sulfide/sulfate, apatite and zircon saturation, and recalculated to 100 wt%

	SiO2	TiO2	Al2O3	Fe2O3	FeO	MnO	MgO	CaO	Na2O	K2O	P2O5	Cr2O3
Start	48.00	1.30	13.00	0.90	8.00	0.23	7.00	10.00	2.40	1.60	0.18	0.13
Melt	51.76	1.40	14.02	0.97	8.63	0.25	7.55	10.78	2.59	1.73	0.19	0.14

Parameters file "C:\Programs\Delphi\Petrolog4\Manual\Tables4.PtlParam" loaded successfully
 C:\Programs\Petrolog4\DemoFiles\Current_data_File.csv loaded successfully

Figure 6.1. 'Reverse crystallisation' option of Petrolog4 interface.

Note: It is recommended that you read Sections 4 and 5 of this Manual before reading this section.

The algorithm for modelling the reverse of fractional crystallisation involves addition of phases that crystallized from the melt back to the melt composition thus moving it up along a cotectic (a liquid line of descent) towards more primitive compositions.

Unlike crystallisation calculations, where crystallisation of any number of phases can be modelled for any starting composition (as the algorithm determines which minerals crystallise from the melt), the phases that are included in the reverse of fractionation calculations must be on the liquidus of the starting composition at the chosen calculation parameters.

Note: Phases that are present on the liquidus of the starting composition can be checked using the 'Melt liquidus association' option (see Section 3 of this Manual).

Unlike crystallisation calculations, where the mineral with the highest pseudo-liquidus temperature is subtracted from the melt composition, the mineral with the lowest pseudo-liquidus temperature is added to the melt composition during reverse of fractionation calculations. The technique is least ambiguous when used with compositions that lie within a single-phase saturation field.

Note: It is possible to calculate the reverse of pure fractional crystallisation only, as equilibrium crystallisation does not preserve sufficient information on the crystallisation history to enable reverse calculations.

Unlike crystallisation calculations, the algorithm for modelling the reverse of fractionation does not have a built-in mechanism for determining when minerals appeared on the liquidus during fractionation, and thus these conditions should be set by the user.

Consider an example with a melt composition having the following crystallisation sequence: first olivine, then plagioclase after 5% crystallisation (crystallisation along an olivine+plagioclase cotectic), and then clinopyroxene after 15% crystallisation (crystallisation along an olivine+plagioclase+clinopyroxene cotectic), with a total extent of crystallisation of 25%. Reversing this crystallisation sequence using the evolved melt composition formed after 25% of crystallisation would start with reversing crystallisation along the olivine+plagioclase+clinopyroxene cotectic. However, the algorithm cannot determine when clinopyroxene (or plagioclase) appeared on the liquidus during fractionation, and the timing of these events should be set by the user. Thus, the calculated trend of melt evolution is dependent on the conditions at which minerals are excluded from calculations to force the trend off a cotectic (refer to Danyushevsky and Plechov, 2011 for further explanations).

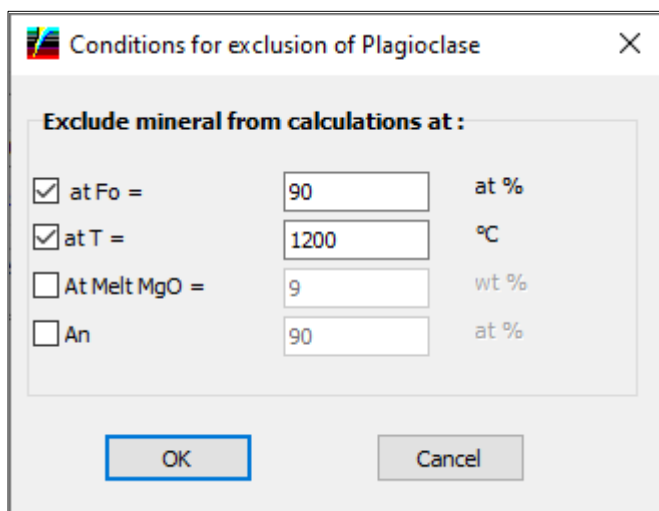


Figure 6.2. The 'Conditions for exclusion' window, showing four available options for specifying timing of plagioclase exclusion from calculations.

The parameters at which the melt moves off a given cotectic (i.e., parameters for phase exclusion) are set in the 'Parameters for Exclusion' subsection of the Parameters section of the Main form (Fig. 6.1). Click on the blue text label ('press to set') next to the desired mineral to open the 'Conditions for exclusion' pop-up window for this mineral (Fig. 6.2).

Petrolog4 offers four different options for setting the timing of exclusion for plagioclase and pyroxenes: 1) temperature; 2) melt MgO content; 3) composition of liquidus olivine; 4) the composition of the phase. For other phases the available options are temperature and melt MgO content. Several options can be set simultaneously, and the mineral will be excluded when one of the set conditions are met. Olivine and spinel cannot be excluded from calculations since primitive melts begin crystallising with olivine and spinel on their liquidus.

Close the window by pressing the 'Ok' button. Pressing the 'Cancel' button closes the window without applying the changes made. The blue label on the Main form will display the chosen option(s).

All other parameters for reverse of fractional crystallisation calculations are set in the same way as for Crystallisation calculation (see Section 4 of this Manual).

Note: The data file can contain columns that contain pressure to be used in calculations and conditions to stop calculations that can differ for each analysis. See section 4.1.10 for more details).

6.1. Saving and loading calculation parameters and structure of output files

Saving and loading calculation parameters is done in the same way as for Crystallisation calculations (see section 4.2).

During reverse of fractional crystallisation calculations, Petrolog4 saves the following files:

FileName_REV__calc_param.csv file lists values of all calculation parameters.

FileName_REV__.csv file contains the starting melt composition, and pseudo-liquidus temperatures and compositional parameters of phases for the selected models.

Note: When exporting results of previous calculations to Excel, the user must click on the FileName_REV__.csv file to initiate export.

Compositions of each phase in equilibrium with the melt are saved in a separate file that have the same naming convention as for Crystallisation calculations (e.g., file FileName_REV_Olv.csv contains olivine compositions).

Note: When 'Add export of elemental concentrations to files' option is used (see Section 1.2), an additional set of files with phase compositions will be added that have '_EL' added at the end of their names (e.g., FileName_REV__EL.csv, FileName_REV_Plg_EL.csv, etc.).

Note: When using user-defined file names, it is recommended to keep file names under 15 characters long, since the length of allowed names for individual sheets in Excel files is limited to 31 characters.

7. Modelling post-entrapment re-equilibration of melt inclusions in olivine

To model post-entrapment re-equilibration of melt inclusions in olivine, chose ‘Olivine MI’ tab of the Main form (Fig. 7.1).

Petrolog 4.2.2 Input from: C:\Programs\Delphi\Petrolog4\Manual\Current_data_File.csv Memory Usage: 1.749 Mb

File Export to MS Excel Tools Help

Crystallisation Reverse Crystallisation Melt Liquidus Association **Olivine MI**

Type of Calculations:
☒ Reconstruct MI composition
☐ Model diffusion profiles

Ol-melt model: [Ford et al. 1983](#) Oxidation state: [Oxygen Buffer: 'QFM'](#)
 Density model: [Lange & Carmichael 1987](#) Fe-Mg diff. model: [Chakraborty 1997](#)

Set of minor elements (Ca, Mn, Cr) in Olivine
☒ Follow model ☐ High-Ca boninites
☐ Komatiites ☐ MORB or BABB

Reconstructing MI composition to a given FeO* content in the trapped melt

Starting melt composition

SiO2	TiO2	Al2O3	Fe2O3	FeO	MnO	MgO	CaO	Na2O	K2O	P2O5	Cr2O3	H2O
48.00	1.00	14.00	0.50	9.00	0.16	7.00	9.00	2.00	0.20	0.22	0.08	3.00

Analysis1

Host olivine composition, Fo: %
 FeO* content in the trapped melt: wt. %

☐ Calculate all analyses from the file [Select another analysis](#) [Set volatile and trace elements*](#)

Model diffusion profiles

Inclusion radius, microns:
 Cooling interval, °C:
☒ Simulate reheating experiment: T exp (°C)

Output to: Ptl_Oltp*_*.csv D values: not set
 Parameters: Program Default Set **Start calculations** **Clear Results** Follow output: ☒ On

Correcting MI in olivine for post-entrapment re-equilibration

The model used for Olv is: Ford et al. 1983
 Fe2O3 in the melt is calculated using QFM buffer of oxygen fugacity following the model of Borisov et al 2018
 Sulfur speciation in the melt is calculated using the model of O'Neill & Navroges 2022
 Calculation Pressure = 1 atm
 Choice for minor elements in olivine (Ca Mn Cr) is: all set to 0
 Os for olivine:

Mineral	H	C+	S-	S+	Cl	O	n/a	Co	Ni	Rb	Sr	Ba	0
olv	0	0	0	0	0	0	0	0	0	0	0	0	0

***** Warning!!!! *****
 The chosen olivine model does not incorporate the effect of H2O and no correction for H2O has been set.

Inclusion No. 1

Start	SiO2	TiO2	Al2O3	Fe2O3	FeO	MnO	MgO	CaO	Na2O	K2O	P2O5	Cr2O3	FeS*_ppm	H2O_wt%	CO2_ppm	S_ppm	SO3_ppm	Cl_ppm	O_wt%	Co_ppm	Ni_ppm	Rb_ppm	Sr_ppm	Ba_ppm
Start	50.89	1.06	14.84	0.53	9.07	0.17	7.42	9.54	2.12	0.21	0.23	0.08	5814.3	3.181	0.0		0.0	72.1	0.010	63.6	97.5	10.6	239.6	64.7
T_run	T_calc	MgO	Fo_h	Fo_c	FeO*f	FeO*m	01%	Melt%	No	Analysis														
1189.7	1189.7	7.41	88.00	82.70	7.00	9.87	0.22	99.78	1	Analysis1														
1189.7	1189.7	7.41	88.00	82.93	7.00	9.72	0.44	99.56	1	Analysis1														
1189.7	1189.7	7.41	88.00	83.17	7.00	9.58	0.66	99.34	1	Analysis1														
1189.7	1189.7	7.41	88.00	83.41	7.00	9.44	0.88	99.12	1	Analysis1														

C:\Programs\Delphi\Petrolog4\Manual\Current_data_File.csv loaded successfully
 12:00:02 AM sec

Figure 7.1. ‘Olivine MI’ option of Petrolog4 interface for reconstructing melt inclusion compositions.

Note: It is recommended to read Sections 4, 5 and 6 of this Manual before reading this section.

7.1. Reconstructing the initial trapped composition of the MI

Re-equilibration of Fe and Mg between melt inclusions and their host olivine phenocrysts is described in detail by Danyushevsky *et al.* (2000a, 2002), with the main points summarised briefly below. The underlying assumption in these considerations is that the composition of the host olivine does not change after trapping of the melt inclusion.

Cooling of an inclusion after trapping results in crystallisation of olivine from the trapped melt, forming an olivine rim on the walls of the inclusion. The crystallising olivine rim is progressively enriched in Fe and depleted in Mg, i.e., becomes poorer in forsterite component, resulting in a compositional gradient within the rim. The existence of this compositional gradient causes re-equilibration of the inclusion with its host. This re-equilibration is achieved by diffusion of Fe out of, and Mg into the initial volume of the inclusion. This leads to a rapid decrease in Fe content of the residual melt inside the inclusion, a process referred to as ‘Fe-loss’ by Danyushevsky *et al.* (2000a).

Conversely, if an olivine grain containing a melt inclusion is heated over the temperature of inclusion entrapment, host olivine around the inclusion would melt, increasing the Mg# of the melt inside the inclusion and resulting in disequilibrium between the melt and host olivine. This leads to re-equilibration of the melt with the host, which is achieved by diffusion of Fe into, and Mg out of the melt inside the

inclusion. This leads to a rapid increase in Fe content of the melt, a process that can be referred to as 'Fe-gain'.

Petrolog4 offers an option of reconstructing the initially trapped melt composition, providing that the user specifies the FeO* content of the trapped melt. The algorithm simulates the following experimental procedure:

- I. An olivine grain containing an inclusion is kept at a given temperature until the inclusion is in complete equilibrium with the host. Within the algorithm, this temperature corresponds to the olivine liquidus temperature of the melt inclusion composition provided (the starting melt composition). The algorithm simulates exchange of Fe and Mg between melt and olivine, which occurs during the re-equilibration process. Re-equilibration may be accompanied by either melting or crystallisation of the host olivine at the inclusion walls.
- II. Once equilibrium is reached, the algorithm compares the FeO* content of the melt with the user-specified FeO* content of the trapped melt.
- III. If the user-specified FeO* content is higher than the FeO* content of the melt, the algorithm simulates increasing experimental temperature while keeping the melt inclusion and its host in equilibrium. If the user-specified FeO* content is lower than the FeO* content of the melt, the algorithm simulates decreasing experimental temperature while keeping the melt inclusion and its host in equilibrium. In both cases this continues until the FeO* content within the melt inclusion equals the user-specified value. The algorithm simulates melting or crystallisation of olivine and the exchange of Fe and Mg between melt and olivine, which occur during this process.

To use this option, click on the 'Reconstruct MI composition' radio button in the 'Type of Calculations' subsection of the Parameters section of the Main form (Fig. 7.1).

The user must provide the composition of the melt inside the inclusion, the composition of the host olivine (Fo, mol%), and the FeO* content of the trapped melt. These parameters are set within the 'Reconstructing MI composition to a given FeO* content of the trapped melt' subsection of the Parameters section of the Main form (Fig. 7.1).

Note: If you would like to load data from a file and use the 'Calculate all analyses from the file' option, the data file must include columns that contain the host olivine composition and the FeO* content of the trapped melt for each analysis. The column names for these two parameters should read 'Fo_h' or 'Fo_fost' and 'FeO_final' or 'FeO_fin' or 'FeO_rock', respectively (not case sensitive).

User-specified calculation parameters for this option include: olivine-melt equilibrium model; melt oxidation state, model for calculating melt density, and a model for calculating minor element contents (Ca, Mn, Cr) in olivine. The first three parameters are set in the same way as described in Section 4 of this Manual. The last parameter allows the user to introduce minor elements into the calculated olivine composition. The contents of these elements are calculated as a function of olivine Fo content, and are set to typical values for either komatiites, or high-Ca boninites, or MORB / BABB. If the contents of these elements in olivine are set to 0 (None), they are modelled as perfectly incompatible elements.

Note: All calculations within this option are performed at a pressure of 1 atm.

During calculations, Petrolog4 records intermediate output in the Output section of the Main form. This output is provided mainly to keep the user informed of the progress of calculations. Petrolog4 writes the results of calculations into output files.

Note: The reconstructed inclusion composition is automatically copied in the 'Model diffusion profiles' subsection of the Parameters section to be used in modelling diffusion profiles if required.

7.1.1. Saving and loading calculation parameters and structure of output files

Saving and loading calculation parameters is done in the same way as for Crystallisation calculations (see Section 4.2).

During reconstructing melt inclusion composition calculations, Petrolog4 saves the following files:

FileName_IRL__calc_param.csv file lists values of all calculation parameters.

FileName_IRS__.csv file contains the main output.

For each inclusion, Petrolog4 writes three lines into the output file. The first line, marked by value '1' in the 'No.' column, corresponds to the starting composition. The second line, marked by value '2' in the 'No.' column, corresponds to the moment when inclusion reaches equilibrium with the host (end of step I above). The third line, marked by value '3' in the 'No.' column, corresponds to the result of the calculations, when inclusion is in equilibrium with the host and the FeO* in the melt matches the user-defined value.

Values in the 'CORR_COEF' column in the output file should be used to calculate the weight concentrations of perfectly incompatible elements in the recalculated inclusion compositions, by multiplying the values in the starting composition by this coefficient. The values in the 'OL_PER' and 'MELT_PER' columns show weight fractions of olivine and the starting melt during calculations (negative values in the 'OL_PER' column indicate melting of olivine from the walls). These values do not represent the final weight percent change to the starting composition, as inclusions are modelled as open systems to allow for Fe/Mg inter-diffusion during calculations.

Note: When exporting results of previous calculations to Excel, the user must click on the FileName_IRL__.csv file to initiate export.

7.2. Modelling diffusive re-equilibration during 'Fe-loss'

Known values of the diffusion coefficient for Fe-Mg inter-diffusion ($D_{\text{Fe-Mg}}$) in olivine allow calculation of the time required for re-equilibration to occur. If an inclusion is completely re-equilibrated, it is possible to calculate the minimum time that the host phenocryst spent at temperatures between trapping and diffusion closure. However, if re-equilibration is not complete when the closure temperature is reached, and thus a diffusion profile around the inclusion is preserved, a quantitative time estimate can be made.

Note: This technique does not allow an estimate of the residence time at (or close to) the trapping temperature, since at these conditions there is no (or very little) crystallisation within the inclusion.

Petrolog4 uses the data from Chakraborty (1997) to calculate the value of $D_{\text{Fe-Mg}}$:

$\text{Lg}(D_{\text{FeMg}}) = -10757/T(\text{K}) - 9.9453 + 0.8063/\text{Fo}$, in sec/m^2 , where Fo is $(\text{Mg}/(\text{Fe}+\text{Mg}))$ in olivine.

Petrolog4 offers an option for forward modelling of the re-equilibration process during cooling after entrapment (i.e., for the case of 'Fe-loss'). To choose this option, press the 'Model diffusion profile' radio button in the 'Type of Calculations' subsection of the Parameters section of the Main form (Fig. 7.2).

The user must provide the trapped inclusion composition, the inclusion radius (microns) and the length of the cooling interval (in °C). These parameters are set within the 'Model diffusion profiles' subsection of the Parameters section of the Main form (Fig. 7.2).

Note: In this option, the starting composition cannot be imported from a data file.

User-specified calculation parameters for this option include: olivine-melt equilibrium model; melt oxidation state, model for calculating melt density, Fe-Mg inter-exchange diffusion model, and a model for calculating minor element contents (Ca, Mn, Cr) in olivine. The first three parameters are set in the exactly the same way as described in Section 2 of this Manual. The last parameter allows the user to introduce minor elements into the calculated olivine composition. The contents of these elements are calculated as a function of olivine Fo content, and are set to typical values for either komatiites, or high-Ca boninites, or MORB / BABB. If the contents of these elements in olivine are set to 0, they are modelled as perfectly incompatible elements.

Note: All calculations within this option are performed at a pressure of 1 atm.

Diffusion modelling can be performed either for the case of instant cooling, or for the case of cooling with a specific cooling rate.

Petrolog 4.2.2 Input from: C:\Programs\Delphi\Petrolog4\Manual\Current_data_File.csv Memory Usage: 1.751 Mb

File Export to MS Excel Tools Help

Crystallisation Reverse Crystallisation Melt Liquidus Association **Olivine MI**

Type of Calculations:

☐ Reconstruct MI composition
☒ Model diffusion profiles

Ol-melt model: [Ford et al. 1983](#) Oxidation state: [Oxygen Buffer: 'QFM'](#)
Density model: [Lange & Carmichael 1987](#) Fe-Mg diff. model: [Chakraborty 1997](#)

Set of minor elements (Ca, Mn, Cr) in Olivine
☒ Follow model ☐ High-Ca boninites
☐ Komatiites ☐ MORB or BABB

Reconstructing MI composition to a given FeO* content in the trapped melt

Host olivine composition, Fo: %
FeO* content in the trapped melt: wt. %

☐ Calculate all analyses from the file

Model diffusion profiles

Starting melt composition

SiO2	TiO2	Al2O3	Fe2O3	FeO	MnO	MgO	CaO	Na2O	K2O	P2O5	Cr2O3	H2O
51.97	1.12	15.62	0.89	6.21	0.18	7.65	10.04	2.23	0.22	0.25	0.09	3.35

☐ Load the result of the last calculation

Type of calculations:

☒ Instant cooling:
(final % of re-equilibration)

☐ Cooling Rate:
(°C/day)

Inclusion radius, microns:
Cooling interval, °C:
☒ Simulate reheating experiment: T exp (°C)

Output to: Ptl_Olpt_*.csv D values: not set

Parameters: Program Default Set

Start calculations Clear Results Follow output: On

Modelling diffusion profiles around MI in olivine. Instant cooling

The model used for Olv is: Ford et al. 1983
Choice for minor elements in olivine (Ca Mn Cr) is: all set to 0
Fe2O3 in the melt is calculated using QFM buffer of oxygen fugacity following the model of Borisov et al 2018
Sulfur speciation in the melt is calculated using the model of O'Neill & Mavrogenes 2002
Calculation Pressure = 1 atm
Melt density is calculated following the model of Lange & Carmichael 1987
Ds for Olivine:

Mineral	H	C+	S-	S+	Cl	O	Co	Ni	Rb	Sr	Ba	e
Olv	0	0	0	0	0	0	n/a	0	0	0	0	0

Cooling interval: 100.00 °C
Extent of re-equilibration: 50.00 %
Inclusion radius: 150.00 micron
Modelling reheating experiment to: 1250.0 °C

***** Warning!!! *****
The chosen olivine model does not incorporate the effect of H2O and no correction for H2O has been set.

Start instant cooling calculations

Calculating melt at 0% re-equilibration; Step 201 completed

Trapping temperature: 1198,

Start complete re-equilibration calculations

Calculating melt at 100% re-equilibration; Step 200 completed; Estimated re-equilibration % = 39.30
Calculating melt at 100% re-equilibration; Step 400 completed; Estimated re-equilibration % = 78.97
Calculating melt at 100% re-equilibration; Step 871 completed; Re-equilibration % = 100.00

Figure 7.2. ‘Olivine MI’ option of Petrolog4 interface for modelling diffusion profiles around melt inclusions. Note that the Debug Section at the bottom of the Main Form is not displayed on this example as Debug output has been switched off by using the ‘DebugOutput On/Off’ item in the ‘Tools’ section of the Main Menu.

7.2.1. Instant cooling calculations

In the case of instant cooling, the zoned rim on the walls of the inclusion grows first and then re-equilibration occurs while the grain resides at the lower end of the cooling interval. To use this option, click on the ‘Instant cooling’ radio button in the ‘Type of calculations’ subsection within the ‘Model diffusion profiles’ subsection in the Parameters section of the Main form (Fig. 7.2). For this option, the user needs to specify the extent of re-equilibration, a parameter that will be used to determine when diffusion calculations are completed. This parameter is set in the text box next to the ‘Instant cooling’ radio button. The degree of re-equilibration, i.e., the extent of ‘Fe-loss’, is defined as the amount of FeO* ‘lost’ by the residual melt relative to the amount that is ‘lost’ in the case of complete re-equilibration.

The output file generated within this option contains the melt compositions and diffusion profiles generated at different stages of calculations. The diffusion profiles are expressed as values of FeO* concentration in olivine over distance from the centre of the melt inclusion. The melt compositions recorded correspond to: 1) the starting composition, 2) the composition of the melt after instant cooling (0% re-equilibration), the composition of the melt in the case of complete re-equilibration (100%), and the composition of the melt at the required extent of re-equilibration. The FeO* profiles recorded correspond to the initial rim profile after the instant cooling, and to the resultant FeO* profile after the calculations are completed.

7.2.2. Cooling rate calculations

In the case of cooling with a specific cooling rate, re-equilibration and cooling occur simultaneously. To use this option, click on the ‘Cooling Rate’ radio button in the ‘Type of calculations’ subsection within the

'Model diffusion profiles' subsection in the Parameters section of the Main form (Fig. 7.2). For this option, the user needs to specify the cooling rate, and the calculations will simulate cooling with the specified rate from the start to the end of the cooling interval. This parameter is set in the text box next to the 'Cooling Rate' radio button.

Modelling of diffusion under this option is performed in 10 °C steps, with each step modelled as a separate instant cooling calculation. The program generates two output files. One file contains a record of diffusion profiles at the end of each 10-degree step, and the second file contains melt compositions at the end of each step. 'PR' at the end of the file name denotes files containing calculated FeO profiles. 'COMP' at the end of the file name denotes files containing calculated melt compositions.

7.2.3. Modelling complex cooling histories

To enable modelling of complex cooling histories, Petrolog4 allows for using the result of the last calculation as the starting point for the next calculation. For this purpose, after each diffusion modelling calculation Petrolog4 saves both the final profile and the final melt composition into a file called 'LAST_RES.DAT'. In order to use the results of the last calculation as the starting point for the following calculation, check the 'Load last result' checkbox in the 'Diffusion profiles modelling' part of the Parameters section of the Main form (Fig. 4.16).

Note: Loading the results of the last calculation automatically sets the size for the inclusion radius, which should not be changed.

Note: It is recommended that the user does not delete file 'LAST_RES.DAT' from the directory which contains the Petrolog4 executable (i.e., 'Petrolog.exe' file).

7.2.4. Simulating reheating experiments

Calculation under both Instant cooling and Cooling rate options can simulate a reheating experiment with the melt inclusions, an optional calculation performed at the end of diffusions modelling. To include this calculation, check the 'Simulate reheating experiment' checkbox within the 'Model diffusion profiles' subsection in the Parameters section of the Main form (Fig. 7.2). The user is then also required to provide a temperature value for the reheating experiment. The temperature is set in the 'T exp (°C)' text box next to the 'Simulate reheating experiment' checkbox.

Using this option allows Petrolog4 to reproduce the following scenario: 1) inclusion is trapped; 2) after entrapment, inclusion is cooled within the plumbing system prior to eruption; 3) the grain with the inclusion is experimentally reheated to a certain temperature and quenched. The results of diffusion modelling can then be directly compared with the analysed composition of the experimentally quenched inclusion.

Note: If the results of a diffusion modelling calculation are intended to be used in the following calculation, simulation of the reheating experiment should not be performed.

7.2.5. Integrating reconstruction of inclusion compositions and diffusion modelling

To facilitate combining calculations of the initial trapped inclusion compositions with diffusion modelling, Petrolog4 populates the Starting melt composition for the 'Model diffusion profiles' option with the result of the calculation performed with the 'Reconstructing MI composition to a given FeO* value' option. Temperature value for experimental reheating is also set to correspond to the olivine liquidus temperature of the starting composition for the 'Reconstructing MI composition to a given FeO* content in the trapped melt'.

Note: It is recommended that the user contacts Petrolog4 support if advanced use of the diffusion modelling is intended.

8. Normative Mineralogy Calculations

To calculate normative mineralogy, chose 'Normative Mineralogy' tab of the Main form (Fig. 8.1).

Note: It is recommended to read Sections 2, 3 and 4 of this Manual before reading this section.

Petrolog 4.2.6 Memory Usage: 1.943 Mb

File Export to MS Excel Tools Help

Crystallisation Reverse Crystallisation Melt Liquidus Association Olivine MI Normative Mineralogy Classifications Development

NORM Calculation Schemes:

- ☐ Le Maitre et al. 2002
- ☐ Petrolog Default
- ☒ Verma et al. 2003
- ☐ Basalt Tetrahedron

Additional Options (if available)

- ☒ use CO2
- ☒ use Na2CO3
- S6+ / Total S : 0.5000

Fe Oxidation State:

- ☐ Fixed Fe3+/Total Fe ratio
- ☐ All Fe as FeO
- ☒ As defined in the composition
- ☐ Middlemost 1989
- ☐ LeMaitre 1976; volcanic
- ☐ LeMaitre 1976; plutonic

Composition

SiO2	TiO2	Al2O3	Fe2O3	FeO	MnO	MgO	CaO	Na2O	K2O	P2O5	Cr2O3	H2O
50.00	1.00	15.00	0.00	9.00	0.10	10.00	12.00	2.50	0.20	0.10	0.10	0.00

[Set volatile and trace elements](#)

PetrologDefault ☐ Calculate all analyses [Select another analysis](#)

Output to: Ptl_Otp4_*.csv D values: not set

Parameters: Program Default Set

Start calculations Clear Results Follow output: On

***** New calculation *****

Normative Mineralogy calculations

The calculation scheme is: Verma et al. 2003

Calculations are performed using FeO and Fe2O3 contents as defined in the starting composition

If CO2 is present in the starting composition, it will be used to form Na2CO3 and calcite

If S is present in the starting composition, normative mineralogy will be calculated using a S6+/(S6+ + S-) value of 0.5000

The composition(s) will be recalculated to 100 wt% including the following trace and volatile elements when their concentrations are defined :

Ni,Co,V,Sr,Ba,Rb,Cs,Li,Zr,F,Cl,S,C

SiO2	TiO2	Al2O3	Fe2O3	FeO	MnO	MgO	CaO	Na2O	K2O	P2O5	Cr2O3	Sample_Number
50.00	1.00	15.00	0.00	9.00	0.10	10.00	12.00	2.50	0.20	0.10	0.10	PetrologDefault

Mineral	Mol_%	Weight_%
Apatite	0.051	0.232
Chromite	0.142	0.147
Ilmenite	2.698	1.899
Kspite	0.915	1.182
Albite	17.385	21.155
Anorthite	22.554	29.118
Cpx	23.053	24.226
Opx	11.538	5.905
Olivine	21.664	16.135

For Chromite, Magnetite and Ilmenite, $100 * Mn / (Mn + Ni + Co + Fe^{2+}) = 1.113$

For Cpx, Opx, Olivine and MagnesioWustite, $100 * Mg / (Mg + Mn + Ni + Co + Fe^{2+}) = 68.611$

Figure 8.1. 'Normative Mineralogy' option of Petrolog4 interface. Note that the Debug Section at the bottom of the Main Form is not displayed on this example as Debug output has been switched off by using the 'DebugOutput On/Off' item in the 'Tools' section of the Main Menu.

8.1. Calculation parameters

Parameters that can be set before starting calculations involve the Calculation Scheme, Fe Oxidation state and some Additional Options depending on the chosen Calculation Scheme.

8.1.1. Choosing a calculation scheme

Choose a Calculation Scheme by selecting one of the options available in the 'NORM Calculation Scheme' subsection of the Parameters Section (Fig. 8.1). The schemes available in this version and a brief description of the 'Petrolog Default' option are listed in Appendix 1.

When the schemes of Le Maitre et al. (2022) or Verma et al. (2003) are chosen, a 'use CO2' checkbox appears in the Additional Options subsection (Fig. 8.1). When the 'use CO2' checkbox is not checked, the CO₂ content of the starting composition will be ignored. When this checkbox is checked and CO₂ is defined in the starting composition, it will be used to form normative carbonates. When using the scheme of Le Maitre et al. (2022), CO₂ will be used to form calcite, followed by magnesite and siderite. When using the scheme of Verma et al. (2003), CO₂ will be used to form calcite. Additionally, the user can decide whether CO₂ will be used to form

Na₂CO₃ by checking the 'use Na₂CO₃' checkbox which is only visible when the 'use CO₂' checkbox is checked. If 'use Na₂CO₃' checkbox is checked, Na₂CO₃ will be formed first, before forming any other carbonates.

When the scheme of Verma et al. (2003) is chosen, a field to enter a value for S⁶⁺/(S⁶⁺ + S⁻) ratio appears in the Additional Options subsection (Fig. 8.1). If sulphur is defined in the starting composition, its content will be split between the oxidised and reduced forms of sulphur using the entered value to form thenardite and pyrite. The default value is 0.5.

8.1.2. Choosing a method to calculate Fe oxidation state

Choose a method to calculate Fe oxidation state by selecting one of the options available in the 'Fe Oxidation State' subsection of the Parameters Section (Fig. 8.1).

Six options for controlling melt oxidation state are available: **I)** calculation with a constant Fe³⁺ / Fe_{total} value; **II)** calculation assuming that all Fe is present as FeO; **III)** using values for Fe₂O₃ and FeO contents that are defined in the starting composition; **IV)** determining Fe₂O₃ and FeO contents using the approach of Middlemost (1989) ; **V)** determining Fe₂O₃ and FeO contents using the approach of Le Maitre (1976) for volcanic rocks; and **VI)** determining Fe₂O₃ and FeO contents using the approach of Le Maitre (1976) for plutonic rocks.

I. When using a constant Fe³⁺ / Fe_{total} value, the contents of Fe₂O₃ and FeO in the starting compositions are recalculated accordingly, before the compositions are normalised to 100 wt%.

II. When assuming that all Fe is present as FeO, the contents of Fe₂O₃ and FeO in the starting compositions are recalculated accordingly, before the compositions are normalised to 100 wt%.

III. When using values for Fe₂O₃ and FeO contents that are defined in the starting composition, no changes are made to the contents of Fe₂O₃ and FeO in the starting compositions.

IV. When the approach of Middlemost (1989) is used, the contents of Fe₂O₃ and FeO in the starting compositions are recalculated based on how the composition is classified on the TAS diagram, as defined by Middlemost (1989), before the compositions are normalised to 100 wt%.

IV. When using Le Maitre (1976) for volcanic rocks, the contents of Fe₂O₃ and FeO in the starting compositions are recalculated following (in wt %) $\text{FeO}/(\text{FeO} + \text{Fe}_2\text{O}_3) = 0.93 - 0.0042 \cdot \text{SiO}_2 - 0.022 \cdot (\text{Na}_2\text{O} + \text{K}_2\text{O})$, before the compositions are normalised to 100 wt%.

IV. When using Le Maitre (1976) for plutonic rocks, the contents of Fe₂O₃ and FeO in the starting compositions are recalculated following (in wt %) $\text{FeO}/(\text{FeO} + \text{Fe}_2\text{O}_3) = 0.88 - 0.0016 \cdot \text{SiO}_2 - 0.027 \cdot (\text{Na}_2\text{O} + \text{K}_2\text{O})$, before the compositions are normalised to 100 wt%.

8.2. Saving and loading calculation parameters and structure of output files

Saving and loading calculation parameters is done in the same way as for Crystallisation calculations (see section 4.2).

During normative mineralogy calculations, Petrolog4 saves the following files:

FileName_NORM__calc_param.csv file lists values of all calculation parameters.

FileName_NORM__.csv file contains the starting composition and calculated normative minerals in molecular and weight proportions.

Note: When 'Add export of elemental concentrations to files' option is used (see Section 1.2), an additional file with the starting composition will be added that have '_EL' added at the end of its name: FileName_NORM__EL.csv.

Note: When exporting results of previous calculations to Excel, the user must click on the FileName_NORM__.csv file to initiate export.

9. Classification diagrams

To classify compositions using available classification diagrams, chose 'Classification' tab of the Main form (Fig. 9.1).

Note: It is recommended to read Sections 2, 3 and 4 of this Manual before reading this section.

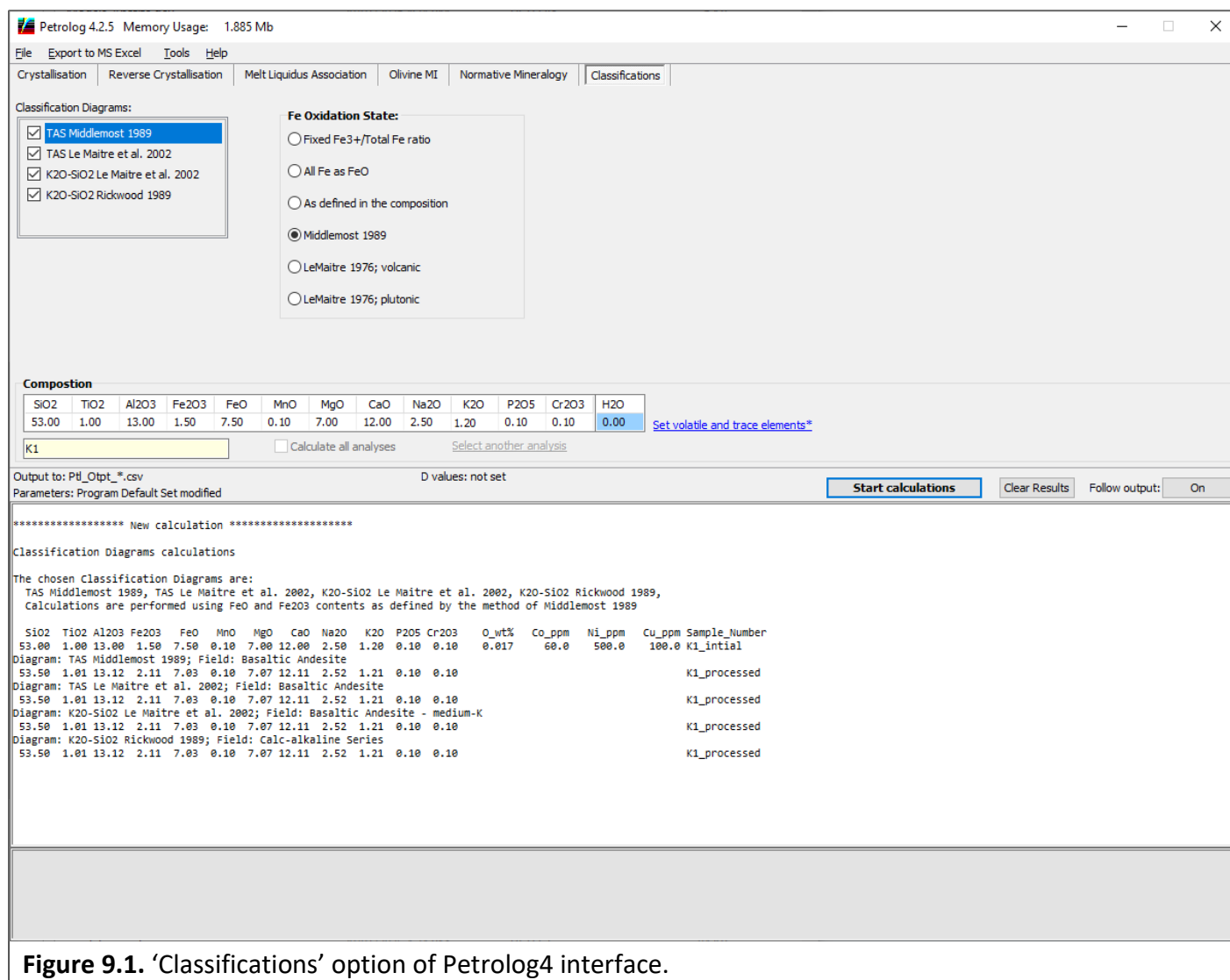


Figure 9.1. 'Classifications' option of Petrolog4 interface.

9.1. Calculation parameters

Parameters that can be set before starting calculations involve the choice of Classification Diagrams and Fe Oxidation state.

9.1.1. Choosing Classification Diagrams

Choose any number of the available Classification Diagrams by checking the desired Classification Diagrams within the 'Classification Diagrams' subsection of the Parameters Section (Fig. 9.1). All Classification Diagrams available in this version are listed in Appendix 1.

9.1.2. Choosing a method to calculate Fe oxidation state

Choose a method to calculate Fe oxidation state by selecting one of the options available in the 'Fe Oxidation State' subsection of the Parameters Section (Fig. 9.1).

Six options for controlling melt oxidation state are available: **I)** calculation with a constant Fe³⁺ / Fe_{total} value; **II)** calculation assuming that all Fe is present as FeO; **III)** using values for Fe₂O₃ and FeO contents that are defined in the starting composition; **IV)** determining Fe₂O₃ and FeO contents using the approach of Middlemost (1989) ; **V)** determining Fe₂O₃ and FeO contents using the approach of Le Maitre (1976) for volcanic rocks; and **VI)** determining Fe₂O₃ and FeO contents using the approach of Le Maitre (1976) for plutonic rocks.

I. When using a constant $\text{Fe}^{3+} / \text{Fe}_{\text{total}}$ value, the contents of Fe_2O_3 and FeO in the starting compositions are recalculated accordingly, before the compositions are normalised to 100 wt%.

II. When assuming that all Fe is present as FeO , the contents of Fe_2O_3 and FeO in the starting compositions are recalculated accordingly, before the compositions are normalised to 100 wt%.

III. When using values for Fe_2O_3 and FeO contents that are defined in the starting composition, no changes are made to the contents of Fe_2O_3 and FeO in the starting compositions.

IV. When the approach of Middlemost (1989) is used, the contents of Fe_2O_3 and FeO in the starting compositions are recalculated based on how the composition is classified on the TAS diagram, as defined by Middlemost (1989), before the compositions are normalised to 100 wt%.

IV. When using Le Maitre (1976) for volcanic rocks, the contents of Fe_2O_3 and FeO in the starting compositions are recalculated following (in wt %) $\text{FeO}/(\text{FeO}+\text{Fe}_2\text{O}_3) = 0.93 - 0.0042*\text{SiO}_2 - 0.022*(\text{Na}_2\text{O} + \text{K}_2\text{O})$, before the compositions are normalised to 100 wt%.

IV. When using Le Maitre (1976) for plutonic rocks, the contents of Fe_2O_3 and FeO in the starting compositions are recalculated following (in wt %) $\text{FeO}/(\text{FeO}+\text{Fe}_2\text{O}_3) = 0.88 - 0.0016*\text{SiO}_2 - 0.027*(\text{Na}_2\text{O} + \text{K}_2\text{O})$, before the compositions are normalised to 100 wt%.

9.2. Saving and loading calculation parameters and structure of output files

Saving and loading calculation parameters is done in the same way as for Crystallisation calculations (see section 4.2).

During Classification Diagrams calculations, Petrolog4 saves the following files:

FileName_CIDg__calc_param.csv file lists values of all calculation parameters.

FileName_CIDg__.csv file contains the starting composition and classification of the starting composition(s) according to the chosen diagram(s).

Note: When 'Add export of elemental concentrations to files' option is used (see Section 1.2), an additional file with the starting composition(s) will be added that have '_EL' added at the end of its name: FileName_CIDg__EL.csv.

Note: When exporting results of previous calculations to Excel, the user must click on the FileName_CIDg__.csv file to initiate export.

References

- Allison CM, Roggensack K, Clarke AB 2019. H₂O–CO₂ solubility in alkali-rich mafic magmas: new experiments at mid-crustal pressures. *Contrib. Mineral. Petrol.* 174 : 58, 24pp. <https://doi.org/10.1007/s00410-019-1592-4>
- Almeev RR, Holtz F, Koepke J, Fleurice P, Botcharnikov RE 2007. The effect of H₂O on olivine crystallization in MORB: Experimental calibration at 200 MPa. *Amer. Mineral.* 92, 670-674.
- Almeev RR, Holtz F, Koepke J, Fleurice P 2012. Experimental calibration of the effect of H₂O on plagioclase crystallization in basaltic melt at 200 MPa. *Amer. Mineral.* 97, 1234-1240.
- Ariskin AA, Barmina GS 1990. Equilibria thermometry between plagioclases and basalt and andesite magmas. *Geochem. Int.* 27(10), 129-134.
- Ariskin AA, Barmina GS 1999. An empirical model for the calculation of spinel-melt equilibria in mafic igneous systems at atmospheric pressure: 2. Fe-Ti oxides. *Contrib. Mineral. Petrol.* 134, 251-263.
- Ariskin AA, Barmina GS, Frenkel MYa 1986. Simulating low-pressure tholeiite-magma crystallization at a fixed oxygen fugacity. *Geokhimiya*, No. 11, 1614-1627; translated into English in *Geochem. Int.* 1987, 24(5), 92-100.
- Ariskin AA, Frenkel MYa, Barmina GS, Nielsen R 1993. COMAGMAT: a Fortran program to model magma differentiation processes. *Comput. Geosci.* 19, 1155-1170.
- Ariskin AA, Nikolaev GS 1996. An empirical model for the calculation of spinel-melt equilibria in mafic igneous systems at atmospheric pressure: 1. Chromian spinels. *Contrib. Mineral. Petrol.* 123, 282-292.
- Beattie P 1993. Olivine-melt and orthopyroxene-melt equilibria. *Contrib. Mineral. Petrol.* 115, 103-111.
- Beattie P, Ford C, Russell D 1991. Partition-Coefficients For Olivine-Melt And Ortho-Pyroxene-Melt Systems. *Contributions to Mineralogy and Petrology* 109, 212-224.
- Blundy JD, Wood BJ 1991. Crystal-chemical controls on the partitioning of Sr and Ba between plagioclase feldspar, silicate melts, and hydrothermal solutions. *Geochim Cosmochim Acta* 55, 193-209.
- Bolikhovskaya SV, Vasil'eva MO, Koptev-Dvornikov EV 1996. Simulating low-Ca pyroxene crystallization in basic systems: new versions of geothermometers. *Geochem. Int.* 33 (12), 1-19.
- Borisov A, Aranovich L, Antoshechkina, P 2025. Zircon solubility in silicate melts: New empirical models and thermodynamics. *Chem. Geology* 679, 122682. <https://doi.org/10.1016/j.chemgeo.2025.122682>
- Borisov A, Behrens H, Holtz F 2018. Ferric/ferrous ratio in silicate melts: a new model for 1 atm data with special emphasis on the effects of melt composition. *Contrib. Mineral. Petrol.* 173, 98.
- Borisov A, Krasheninnikov S, Almeev R, Holtz F 2025. Ferric/ferrous ratio in silicate melts: a model calibrated for felsic compositions. *Contrib. Mineral. Petrol.* 180, 89.
- Borisov AA, Shapkin AI 1990. A new empirical equation rating Fe³⁺/Fe²⁺ in magmas to their composition, oxygen fugacity, and temperature. *Geochem. Int.* 27, 111-116.
- Bottinga Y, Weill DF 1972. The viscosity of magmatic silicate liquids: a model for calculation. *Amer. J. Sci.* 272, 438-475.
- Boulliung J, Wood BJ 2023. Sulfur oxidation state and solubility in silicate melts. *Contrib. Mineral. Petrol.* 178, 56. <https://doi.org/10.1007/s00410-023-02033-9>
- Bychkov D.A. CryMinal program and a set of compositometers: tools for modeling equilibria between silicate melts and minerals (in Russian) Ph. D. thesis. Moscow, 2023, 139pp., available at: <https://dissovet.msu.ru/download/f2692eec-f3b4-11ed-87b7-005056b96f20>
- Chakraborty S 1997. Rates and mechanisms of Fe-Mg interdiffusion in olivine at 980°-1300°. *Journal of Geophysical Research-Solid Earth* 102, 12317-12331.
- Crisp LJ, Berry AJ 2022. A new model for zircon saturation in silicate melts. *Contrib. Mineral. Petrol.* 177, 71. <https://doi.org/10.1007/s00410-022-01925-6>
- Danyushevsky LV 2001. The effect of small amounts of H₂O on crystallisation of mid-ocean ridge and backarc basin magmas. *J. Volcan. Geoth. Res.* 110, 265-280.
- Danyushevsky LV, Della-Pasqua FN, Sokolov S 2000a. Re-equilibration of melt inclusions trapped by magnesian olivine phenocrysts from subduction-related magmas: petrological implications. *Contrib. Mineral. Petrol.* 138, No.1, 68-83.

- Danyushevsky LV, Plechov P 2011. Petrolog3: Integrated software for modeling crystallization processes. *Geochem. Geophys. Geosyst.* 12, Q07021.
- Danyushevsky LV, Sokolov S, Falloon TJ 2002: Melt inclusions in olivine phenocrysts: using diffusive re-equilibration to determine the cooling history of a crystal, with implications for the origin of olivine-phyric volcanic rocks. *J. Petrology* 43, 1651-1671.
- Ding S, Plank T, Wallace PJ, Rasmussen DJ 2023. Sulfur_X: A Model of Sulfur Degassing During Magma Ascent. *Geochem. Geophys. Geosyst.* 24, e2022GC010552. <https://doi.org/10.1029/2022GC010552>
- Ding S, Hough T, Dasgupta R 2018. New high-pressure experiments on sulfide saturation of high-FeO* basalts with variable TiO₂ contents – Implications for the sulfur inventory of the lunar interior. *Geochim. Cosmochim. Acta* 222, 319-339.
- Dixon JE 1997. Degassing of alkalic basalts. *Amer. Mineral.* 82, 368-378.
- Drake MJ 1976. Plagioclase-melt equilibria. *Geochim. Cosmochim. Acta* 40, 457-465.
- Falloon TJ, Danyushevsky LV 2000. Melting of refractory mantle at 1.5, 2.0 and 2.5 GPa under H₂O-undersaturated conditions: implications for the petrogenesis of high-Ca boninites and the influence of subduction components on mantle melting. *J. Petrology* 41, 257-283.
- Falloon TJ, Green DH 1988. Anhydrous partial melting of peridotite from 8 to 35 kbars and the petrogenesis of MORB. *J. Petrology Special Issue "Oceanic and Continental Lithosphere: Similarities and Differences"*, 379-414.
- Ford CE, Russell DG, Groven JA, Fisk MR 1983. Distribution coefficients of Mg²⁺, Fe²⁺, Ca²⁺ and Mn²⁺ between olivine and melt. *J. Petrol.* 24, 256-265.
- Fortin MA, Riddle J, Desjardins-Langlais Y, Baker DR 2015. The effect of water on the sulfur concentration at sulfide saturation (SCSS) in natural melts. *Geochim Cosmochim Acta* 160, 100-116.
- Frost BR 1991. Introduction to oxygen fugacity and its petrologic importance. In: *Reviews in Mineralogy*, v25, 1-10.
- Gaetani GA, Watson EB 2002. Modelling the major-element evolution of olivine-hosted melt inclusions. *Chem. Geology* 183, 25-41.
- Giordano D, Dingwell DB 2003. Non-Arrhenian multicomponent melt viscosity: a model. *Earth and Planetary Science Letters* 208, 337-349.
- Herzberg C, O'Hara MJ 2002. Plume-associated ultramafic magmas of phanerozoic age. *J. Petrol.* 43, 1857-1883.
- Hirschmann MM 2021. Iron-wüstite revisited: A revised calibration accounting for variable stoichiometry and the effects of pressure. *Geochim Cosmochim Acta* 313, 74-84. <https://doi.org/10.1016/j.gca.2021.08.039>
- Holloway JR, Blank JG 1994. Application of experimental results to C–O–H species in natural melts. In M.R. Carroll and J.R. Holloway (Eds.), *Volatiles in Magmas* (Rev. Mineral., 30, pp. 187–230).
- Hughes EC, Liggins P, Saper L, Stolper EM 2024. The effects of oxygen fugacity and sulfur on the pressure of vapor-saturation of magma. *American Mineralogist* 109, 422–438.
- Iacono-Marziano G, Morizet Y, Le Trong E, Gaillard F 2012. New experimental data and semi-empirical parameterization of H₂O–CO₂ solubility in mafic melts. *Geochim. Cosmochim. Acta* 97, 1-22.
- Iacovino K 2022. Calculate fO₂ Buffer. <https://doi.org/10.5281/zenodo.5907867>
- Iacovino K, Till CB 2019. DensityX: A program for calculating the densities of magmatic liquids up to 1,627 °C and 30 kbar. *Volcanica* 2(1), 1-10. <https://doi.org/10.30909/vol.02.01.0110>
- Jugo PJ 2009. Sulfur content at sulfide saturation in oxidized magmas. *Geology* 37, 415-418.
- Kilinc A, Carmichael ISE, Rivers ML, Sack RO 1983. The ferric-ferrous ratio of natural silicate liquids equilibrated in air. *Contrib. Mineral. Petrol.* 83, 136-140.
- Kinzler RJ, Grove TL, Recca SI 1990. An Experimental-Study on the Effect of Temperature and Melt Composition on the Partitioning of Nickel Between Olivine and Silicate Melt. *Geochim Cosmochim. Acta* 54, 1255-1265.
- Kiseeva ES, Wood BJ 2015. The effects of composition and temperature on chalcophile and lithophile element partitioning into magmatic sulphides. *Earth and Planetary Science Letters* 424, 280–294.
- Koch L, Almeev RR, Linsler SA, Marxer F, Holtz F 2025. The effect of H₂O on the crystallization of orthopyroxene in a high-Mg andesitic melt. *Amer. Mineral.* in press. <https://doi.org/10.2138/am-2024-9593>.

- Koshlyakova AN, Sobolev AV, Krashenninnikov SP, Batanova VG, Borisov AA 2022. Ni partitioning between olivine and highly alkaline melts: An experimental study. *Chem. Geology* 587, 120615. <https://doi.org/10.1016/j.chemgeo.2021.120615>.
- Kress VC, Carmichael ISE 1988. Stoichiometry of the iron oxidation reaction in silicate melts. *Amer. Mineral.* 73, 1267-1274.
- Kress VC, Carmichael ISE 1991. The compressibility of silicate liquids containing Fe₂O₃ and the effect of composition, temperature, oxygen fugacity and pressure on their redox states. *Contrib. Mineral. Petrol.* 108 82-92.
- Lange RA, Carmichael ISE 1987. Densities of Na₂O-K₂O-CaO-MgO-FeO-Fe₂O₃-Al₂O₃-TiO₂-SiO₂ liquids: New measurements and derived partial molar properties. *Geochim. Cosmochim. Acta* 51, 2931-2946.
- Langmuir CH, Klein EM, Plank T 1992. Petrological systematics of Mid-Ocean Ridge Basalts: Constraints on melt generation beneath ocean ridges. In: *Mantle flow and melt generation at mid-ocean ridges*. AGU Geophysical Monograph 71, pp. 183-280.
- Le Maitre RW, Streckeisen A, Zanettin B, Le Bas MJ, Bonin B, Bateman P, eds. 2002. *Igneous Rocks: A Classification and Glossary of Terms: Recommendations of the International Union of Geological Sciences Subcommission on the Systematics of Igneous Rocks*. 2nd ed. Cambridge University Press, 236 pp. DOI: <https://doi.org/10.1017/CBO9780511535581>
- Le Maitre RW 1976. Some Problems of the Projection of Chemical Data into Mineralogical Classifications. *Contrib. Mineral. Petrol.* 56, 181-189.
- Lesne P, Scaillet B, Pichavant M, Iacono-Marziano G, Beny JM 2011. The H₂O solubility of alkali basalts: an experimental study. *Contrib. Mineral. Petrol.* 162, 133–151. <https://doi.org/10.1007/s00410-010-0588-x>
- Li C, Ripley EM 2005. Empirical equations to predict the sulfur content of mafic magmas at sulfide saturation and applications to magmatic sulfide deposits. *Mineralium Deposita* 40, 218-230.
- Li C, Ripley EM 2009. Sulfur Contents at Sulfide-Liquid or Anhydrite Saturation in Silicate Melts: Empirical Equations and Example Applications. *Econom. Geol.* 104, 405-412.
- Lindsley DH (ed) 1991. *Oxide Minerals: Petrologic and Magnetic Significance*. *Reviews in Mineralogy*, v. 25.
- Lundgaard KL, Tegner C 2004. Partitioning of ferric and ferrous iron between plagioclase and silicate melt. *Contrib. Mineral. Petrol.* 147, 470-482. [https:// DOI 10.1007/s00410-004-0568-0](https://doi.org/10.1007/s00410-004-0568-0).
- Medard E, Grove TL 2008. The effect of H₂O on the olivine liquidus of basaltic melts: Experiments and thermodynamic models. *Contrib. Mineral. Petrol.* 155, 417-432.
- Middlemost EAK 1989. Iron oxidation ratios, norms and the classification of volcanic rocks. *Chemical Geology*, 77, 19-26.
- Moore G, Vennemann T, Carmichael ISE 1998. An empirical model for the solubility of H₂O in magmas to 3 kilobars. *American Mineralogist* 83, 36-42.
- Nash WM, Smythe DJ, Wood BJ 2019. Compositional and temperature effects on sulfur speciation and solubility in silicate melts. *Earth and Planetary Science Letters* 507, 187-198.
- Nathan HD, Vankirk CK 1978. A model of magmatic crystallisation. *J. Petrol.* 19, 66-94.
- Newman S, Lowenstern JB 2002. VolatileCalc: a silicate melt–H₂O–CO₂ solution model written in Visual Basic for excel. *Computers and Geosciences* 28, 597–604.
- Nelson SA, Carmichael ISE 1979. Partial Molar Volumes of Oxides Component in Silicate Liquids. *Contrib. Mineral. Petrol.* 71, 117-124.
- Nielsen RL 1985. EQUIL: A program for the modeling of low-pressure differentiation processes in natural mafic magma bodies. *Computers and Geosciences* 11, 531-546.
- Nielsen RL 1988. TRACE.FOR: A program for the calculation of combined major and trace-element liquid lines of descent for natural magmatic systems. *Computers and Geosciences* 14, 15-35.
- Nielsen RL, Drake MJ 1979. Pyroxene-melt equilibria. *Geochim. Cosmochim. Acta* 43, 1259-1272.
- Nielsen RL, Dungan MA 1983. Low pressure mineral-melt equilibria in natural anhydrous mafic systems. *Contrib. Mineral. Petrol.* 84, 310-326.
- O'Neill HStC 2021. The Thermodynamic Controls on Sulfide Saturation in Silicate Melts with Application to Ocean Floor Basalts. *Magma Redox Geochemistry, Geophysical Monograph* 266, 177-213.
- O'Neill HStC, Mavrogenes JA 2022. The sulfate capacities of silicate melts. *Geochim. Cosmochim. Acta* 334, 368-382.

- Pletchov PYu, Gerya TV 1998. Effect of H₂O on plagioclase-melt equilibrium. *Experiment in GeoSciences* 7, No. 2, 7-9.
- Plechov PYu, Shchekleina MD, Dymshits AM 2023. Modelling of Quartz-Melt equilibrium in simple and complex silicate systems. *New Data for Minerals*, 4, 110-118, doi: 10.25993/FM.2023.57.2023.012
- Putirka KD 2005. Mantle potential temperatures at Hawaii, Iceland, and the mid-ocean ridge system, as inferred from olivine phenocrysts: Evidence for thermally driven mantle plumes. *Geochem. Geophys. Geosyst.* 6. Q05L08.
- Putirka KD 2008. Thermometers and Barometers for Volcanic Systems. *Reviews in Mineralogy & Geochemistry*, 69, 61-120. DOI: 10.2138/rmg.2008.69.3.
- Putirka KD, Perfit M, Ryerson FJ, Jackson MG 2007. Ambient and excess mantle temperatures, olivine thermometry, and active vs. passive upwelling. *Chemical Geology* 241, 177–206. doi:10.1016/j.chemgeo.2007.01.014
- Rickwood PC 1989. Boundary lines within petrologic diagrams which use oxides of major and minor elements. *Lithos* 22, 247-263.
- Roeder PL, Emslie RF 1970. Olivine-liquid equilibrium. *Contrib. Mineral. Petrol.* 29, 275-89.
- Sack RO, Carmichael ISE, Rivers ML, Ghiorso MS 1980. Ferric-ferrous equilibria in natural silicate liquids at 1 bar. *Contrib. Mineral. Petrol.* 75, 369-376.
- Shishkina TA, Botcharnikov RE, Holtz F, Almeev RR, Jazwa AM, Jakubiak AA 2014. Compositional and pressure effects on the solubility of H₂O and CO₂ in mafic melts. *Chem. Geology* 388, 112-129. <http://dx.doi.org/10.1016/j.chemgeo.2014.09.001>
- Smythe DJ, Wood BJ, Kiseeva ES 2017. The S content of silicate melts at sulfide saturation: New experiments and a model incorporating the effects of sulfide composition. *American Mineralogist*, Volume 102, pages 795–803. <http://dx.doi.org/10.2138/am-2017-5800CCBY>
- Sobolev AV, Slutskiy AB 1984. Composition and crystallisation conditions of the initial melt of the Siberian meimechites in relation to the general problem of the ultrabasic magmas. *Soviet Geology and Geophysics* 25, 93-104.
- Sun C, Yao L 2024. Redox equilibria of iron in low- to high-silica melts: A simple model and its applications to C-H-O-S degassing. *Earth and Planetary Science Letters*, 638, 118742. doi.org/10.1016/j.epsl.2024.118742
- Tollari N, Toplis MJ, Barnes S-J 2006. Predicting phosphate saturation in silicate magmas: An experimental study of the effects of melt composition and temperature. *Geochimica et Cosmochimica Acta*, 70, 1518–1536. doi:10.1016/j.gca.2005.11.024.
- Toplis MJ 2005. The thermodynamics of iron and magnesium partitioning between olivine and liquid: criteria for assessing and predicting equilibrium in natural and experimental systems. *Contrib. Mineral. Petrol.* 149, 22-39.
- Verma SP, Torres-Alvarado IS, Velasco-Tapia F 2003. A revised CIPW norm. *Schweizerische Mineralogische und Petrographische Mitteilungen*, 83, 197–216.
- Wallace P, Carmichael ISE 1992. Sulfur in basaltic magmas. *Geochimica et Cosmochimica Acta* 56, 1863-1874.
- Waters LE, Lange RA 2015. An updated calibration of the plagioclase-liquid hygrometer-thermometer applicable to basalts through rhyolites. *American Mineralogist*, 100, 2172–2218. <http://dx.doi.org/10.2138/am-2015-5232>
- Weaver JS, Langmuir CH 1990. Calculation of phase equilibrium in mineral-melt systems. *Computers and Geosciences* 16, 1-19.
- Wood DJ, Blundy JD 1997. A predictive model for rare earth element partitioning between clinopyroxene and anhydrous silicate melt. *Contrib. Mineral. Petrol.* 129, 166-181.
- Zajacz Z, Tsay A 2019. An accurate model to predict sulfur concentration at anhydrite saturation in silicate melts. *Geochimica et Cosmochimica Acta*, 261, 288–304. doi: 10.1016/j.gca.2019.07.007

Appendix 1. List of available models and other technical information

Olivine-melt equilibrium models: Ariskin et al. 1986; Ariskin et al. 1993; Beattie 1993; Bychkov 2023; Danyushevsky 2001; Ford et al. 1983; Gaetani and Watson 2002; Herzberg and O'Hara 2002; Langmuir et al. 1992; Nathan and Vankirk 1978; Nielsen 1985; Nielsen 1988; Putirka 2005; Putirka 2008; Putirka et al. 2007; Roeder and Emslie 1970; Sobolev and Slutskiy 1984; Weaver and Langmuir 1990.

Olivine-melt Fe-Mg exchange Kd models: $K_d = \text{const}'$; $\ln(K_d) = A/T(K) + B \cdot P(\text{kbar})/T(K) + C'$; Sobolev and Danyushevsky 1994; Toplis 2005.

Plagioclase-melt equilibrium models: Ariskin and Barmina 1990; Ariskin et al. 1993; Bychkov 2023; Danyushevsky 2001; Drake 1976; Langmuir et al. 1992; Nathan and Vankirk 1978; Nielsen 1985; Nielsen and Dungan 1983; Plechov and Gerya 1998; Waters and Lange 2015; Weaver and Langmuir 1990.

Clinopyroxene-melt equilibrium models: Ariskin et al. 1986; Ariskin et al. 1993; Bychkov 2023; Danyushevsky 2001; Langmuir et al. 1992; Nathan and Vankirk 1978; Nielsen 1985; Nielsen 1988; Nielsen and Drake 1979; Weaver and Langmuir 1990.

Orthopyroxene-melt equilibrium models: Ariskin et al. 1993; Beattie 1993; Bolikhovskaya et al. 1995; Bychkov 2023; Nathan and Vankirk 1978; Nielsen and Drake 1979.

Pigeonite-melt equilibrium models: Ariskin et al. 1986; Ariskin et al. 1993; Bolikhovskaya et al. 1995; Bychkov 2023; Nielsen 1988.

Spinel-melt equilibrium models: Ariskin and Nikolaev 1996; Nielsen 1985.

Ilmenite-melt equilibrium models: Ariskin and Barmina 1999; Nielsen 1985.

Magnetite-melt equilibrium models: Ariskin and Barmina 1999; Nathan and Vankirk 1978.

Quartz-melt equilibrium models: Nathan and Vankirk 1978; Plechov et al. 2023.

Orthoclase-melt equilibrium models: Nathan and Vankirk 1978.

Nepheline-melt equilibrium models: Nathan and Vankirk 1978.

Leucite-melt equilibrium models: Nathan and Vankirk 1978.

Sulphide melt- silicate melt equilibrium models: Kiseeva and Wood 2015; O'Neill 2021; pure FeS.

Sulphate melt- silicate melt equilibrium models: pure anhydride (CaSO_4).

Fluid-melt equilibrium models: Allison et al. 2019; Dixon 1997; Holloway and Blank 1994; Hughes et al., 2024 (pure H_2O - CO_2 fluid); Iacono-Marziano et al. 2012; Newman and Lowenstern 2002 (VolatileCalc); pure H_2O ; pure CO_2 .

Apatite-melt equilibrium models: pure apatite ($\text{Ca}_5\text{P}_3\text{O}_{12.5}$).

Zircon-melt equilibrium models: pure zircon (ZrSiO_4).

Models for setting H_2O corrections to calculated temperatures:

Olivine: Almeev et al. 2007; Danyushevsky 2001; Medard and Grove 2008.

Plagioclase: Almeev et al. 2012; Danyushevsky 2001.

Orthopyroxene: Koch et al. 2025.

Sulphide saturation models: Ding et al. 2018; Fortin et al. 2015; Li and Ripley 2005; Li and Ripley 2009; O'Neill 2021; Smythe et al. 2017; Wallace and Carmichael 1992; No S saturation.

Sulphate saturation models: Zajacz and Tsay 2019.

Fluid saturation models: Allison et al. 2019; Dixon 1997; Holloway and Blank 1994; Iacono-Marziano et al. 2012; Lesne et al. 2011; Moore et al. 1998; Newman and Lowenstern 2002; Shishkina et al. 2014.

Apatite saturation models: Tollari et al. 2006; No Ap saturation.

Zircon saturation models: Borisov et al. 2025; Crisp and Berry 2022; No Zr saturation.

Models of Fe oxidation state in the melt: Borisov and Shapkin 1990; Borisov et al. 2018; Borisov et al. 2025; Kilinc et al. 1983; Kress and Carmichael 1988; Kress and Carmichael 1991; Sack et al. 1980; Sun and Yao 2024.

Models of S oxidation state in the melt: Boulliang and Wood 2023; Jugo 2009; Nash et al. 2019; O'Neill and Mavrogenes 2022; Sun and Yao 2024.

Melt density models: Iacovino and Till 2019; Lange and Carmichael 1997; Nelson and Carmichael 1979

Melt viscosity models: Giordano and Dingwell 2003; Bottinga and Weill 1972.

Models for trace element distribution coefficients between a phase and the silicate melt:

Olivine: Beattie et al. 1991 (Ni and Co); Kinzler et al. 1990 (Ni); Koshlyakova et al. 2022 (Ni);

Plagioclase: Blundy and Wood 1991 (Ba and Sr)

Clinopyroxene: Wood and Blundy 1997 (Y and REE)

Fluid: Ding et al. 2023 (S^{2-} and S^{6+}).

Normative Mineralogy calculation schemes:

Le Maitre et al. 2002; Petrolog default; Verma et al. 2003; Basalt Tetrahedron (after Falloon and Green 1988).

Classification diagrams:

Le Maitre et al. 2002 TAS; Le Maitre et al. 2002 K₂O-SiO₂; Middlemost 1989 TAS; Rickwood 1989 K₂O-SiO₂.

Petrolog4 default corrections to the calculated pseudo-liquidus temperature for the effect of melt H₂O content: The corrections are power functions $dT (^{\circ}C) = A * (H_2O \text{ wt.}\%)^B$ with the following coefficients:

Feldspars and Quartz: A = 121.75 B = 0.512;

Orthopyroxene: A = 100.0 B = 0.45;

Clinopyroxenes: A = 90.0 B = 0.37;

Olivine, Oxides and Feldspathoids: A = 74.404 B = 0.352.

Petrolog4 default corrections to the calculated pseudo-liquidus temperature for the effect of pressure:

The corrections are linear functions with the following slopes:

Pyroxenes: 10 °/kbar;

All other minerals: 5 °/kbar.

Petrolog4 default Normative mineralogy calculation scheme:

The scheme uses only the major elements (see Section 1) and involves the following minerals: Apatite, Magnetite, Chromite, Ilmenite, Rutile, Potassium Feldspar, Leucite, Kaliophilite, Albite, Nepheline, Anorthite, Corundum, Wollastonite, Larnite, Quartz, Clinopyroxene, Orthopyroxene, Olivine, MagnesioWustite.

If a composition cannot be represented by the above set of minerals, calculations are aborted and a message is displayed explaining the reason for aborting calculation.

When norms of Magnetite, Chromite and Ilmenite are calculated, all available Mn and Fe²⁺ are combined and 100*Mn/(Mn+Fe²⁺) is reported. When norms of Clinopyroxene, Orthopyroxene, Olivine and MagnesioWustite are calculated, all available Mg, Mn and Fe²⁺ are combined and 100*Mg/(Mg+Mn+Fe²⁺) are reported.

Oxygen buffers:

Iron-wustite buffer from Hirschmann (2021).

Buffer equations from Iacovino (2022) based on Frost (1991):

$\text{Lg } f\text{O}_2 = A / \text{TK} + B + C * (\text{P}_{\text{bar}} - 1) / \text{TK}$			
Buffer	A	B	C
QFe	-29520.8	7.492	0.05
Fe-W	-27489	6.702	0.055
WM	-32807	13.012	0.083
Co-CoO	-24332.6	7.295	0.052
QFM	-25096.3	8.735	0.11
Ni-NiO	-24930	9.36	0.046
MH	-25700.6	14.558	0.019

Atomic weights (amu) and charges (all atomic weights from <https://iupac.qmul.ac.uk/AtWt/> "ATOMIC WEIGHTS OF THE ELEMENTS 2021"; * S+ has a charge of +4 in fluid):

	Si	Ti	Al	Fe3	Fe2	Mn	Mg	Ca	Na	K	P	Cr
Atomic wt.	28.09	47.88	26.98	55.85	55.85	54.94	24.31	40.08	22.99	39.1	30.97	52
Charge	4	4	3	3	2	2	2	2	1	1	5	3

	H	C+	S-	S+	Cl	O	Li	B	Be	Sc	V	Co
Atomic wt.	1.008	12.01	32.06	32.06	35.45	16	6.94	10.81	9.01	44.96	50.94	58.93
Charge	1	4	-2	6 *	0	-2	1	3	2	3	3	2

	Ni	Cu	Zn	Ga	Rb	Sr	Y	Zr	Nb	Ru	Rd	Pd
Atomic wt.	58.69	63.55	65.39	69.72	85.47	87.62	88.91	91.22	92.91	101.1	102.9	106.4
Charge	2	1	2	3	1	2	3	4	5	4	4	4

	Cs	Ba	La	Ce	Pr	Nd	Sm	Eu	Gd	Tb	Dy	Ho
Atomic wt.	132.9	137.3	138.9	140.1	140.9	144.2	150.4	152	157.2	158.93	162.5	164.9
Charge	1	2	3	3	3	3	3	3	3	3	3	3

	Er	Tm	Yb	Lu	Hf	Ta	Re	Os	Ir	Pt	Pb	Th	U
Atomic wt.	167.3	168.9	173	175	178.5	180.9	186.2	190.2	192.2	195.1	207.2	232	238
Charge	3	3	3	3	4	5	4	4	4	4	2	4	4

Redox equilibria:

